



# Models and Information Integration in Multichannel Radar Remote Sensing Imagery

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**IGARSS 2007  
Tutorial**



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## Summary



- Introduction
  - One Dimensional SAR Systems
    - Synthetic Aperture Radar Principles
    - Scatterer Models
    - Wave Scattering Models. Interaction with Matter
    - SAR Data Models and Speckle Noise
  - Multidimensional SAR Systems
  - Multidimensional SAR Data Models
  - Multidimensional SAR Speckle Noise Models
    - Coherence Modelling and Estimation
    - Polarimetric Information Estimation
    - Multidimensional SAR Data Estimation
    - PolInSAR Data Estimation
- Part 1
- Part 2

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Introduction



- Why to use **Synthetic Aperture Radar** to perform **remote sensing**?
  - Active system providing its own illumination source. Day/night imaging capability (x2)
  - Imaging capability independent of weather conditions (~ x5)
  - High spatial resolution
  - Sensitive to a wide range of **Earth surface properties**, especially in the case of **multichannel** or **multidimensional** SAR systems
    - Interferometry, differential interferometry, polarimetry, polarimetric interferometry, multifrequency, multitime, etc...
- SAR technology has been considered in different applications
  - Topography, agriculture, forestry, hydrology, oceanography, glaciology, environment monitoring, MTI, etc...
- Complementary to **optical** remote sensing systems



ERS 2 (Composite Image)



?  
Band 1: 5.86 cm

Landsat Thematic Mapper (TM)



?  
Band 1: 0.45 - 0.52  $\mu\text{m}$   
Band 2: 0.52 - 0.60  $\mu\text{m}$   
Band 3: 0.63 - 0.69  $\mu\text{m}$   
Band 4: 0.76 - 0.90  $\mu\text{m}$   
Band 5: 1.55 - 1.75  $\mu\text{m}$   
Band 6: 10.40 - 12.50  $\mu\text{m}$   
Band 7: 2.08 - 2.35  $\mu\text{m}$

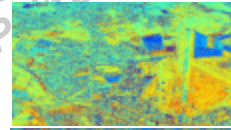
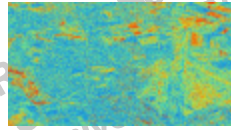
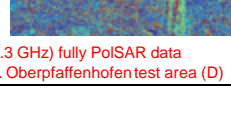
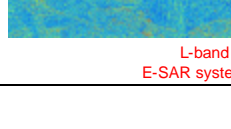


Multidimensional SAR systems exploit **diversity** to increase the amount of information

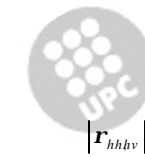
- Multiple channels of information, i.e., PolSAR images


 $|S_{hh}|$ 
 $|S_{hv}|$ 
 $|S_{vv}|$ 

- Correlation between the different PolSAR images

 $|r_{hhvv}|$ 

 $q_{hhvv}$ 
 $|r_{hhhv}|$ 

 $q_{hhhv}$ 

$$r_{k,l} = \frac{E\{S_k \cdot S_l^* \}}{\sqrt{E\{|S_k|^2\} \cdot E\{|S_l|^2\}}} = |r_{k,l}| e^{j\theta_{k,l}}$$



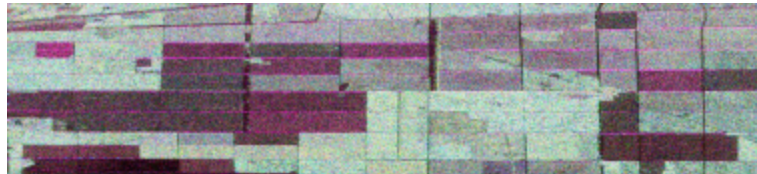
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L-band (1.3 GHz) fully PolSAR data  
E-SAR system, Oberpfaffenhofentest area (D)

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Multifrequency configurations sensitive to different properties of the scatterers



P-Band



L-Band



C-Band

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$|Shh|$   $|Shv|$   $|Svv|$

JPL AIRSAR Nezer Forest Data8

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**Introduction** Synthetic Aperture Radar

Interferometric configurations sensitive to the terrain's topography

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**Introduction** Information Extraction

What do we mean by information extraction ?

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Impact on Remote Sensing due to speckle



### Nature of the extracted information

- **Qualitative** information: Refers to relative information. The interest focuses on retrieving information concerning physical parameters that may describe, or even to distinguish different areas of the SAR data
  - Classification techniques
- **Quantitative** information: Refers to absolute information. The interest is on the retrieval of geophysical and biophysical parameters to describe the Earth surface and its dynamics
  - Inverse Problem
  - Electromagnetic modelling



### What do they mean and which advantages provide **data models** ?

- A (better) **description** of the data acquired by the SAR system, making possible the (better) **extraction** of useful information
- Data can be **systematically** interpreted
- Allow a **generalization** of the observations
- Make possible to deal with the **complexity** associated with the scattering process
- In the lack of data models, only a **phenomenological interpretation** is possible

### SAR data models are:

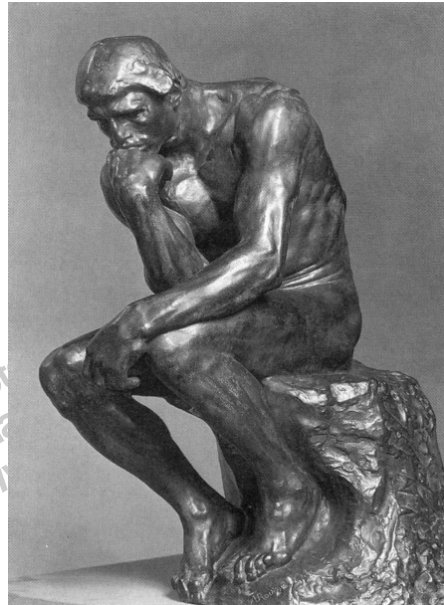
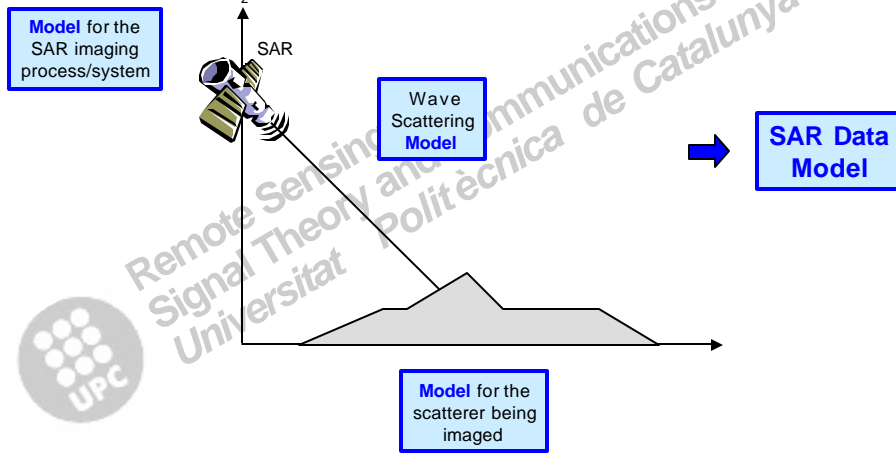
- Controlled by a set of **parameters**
- **Stochastic** in nature

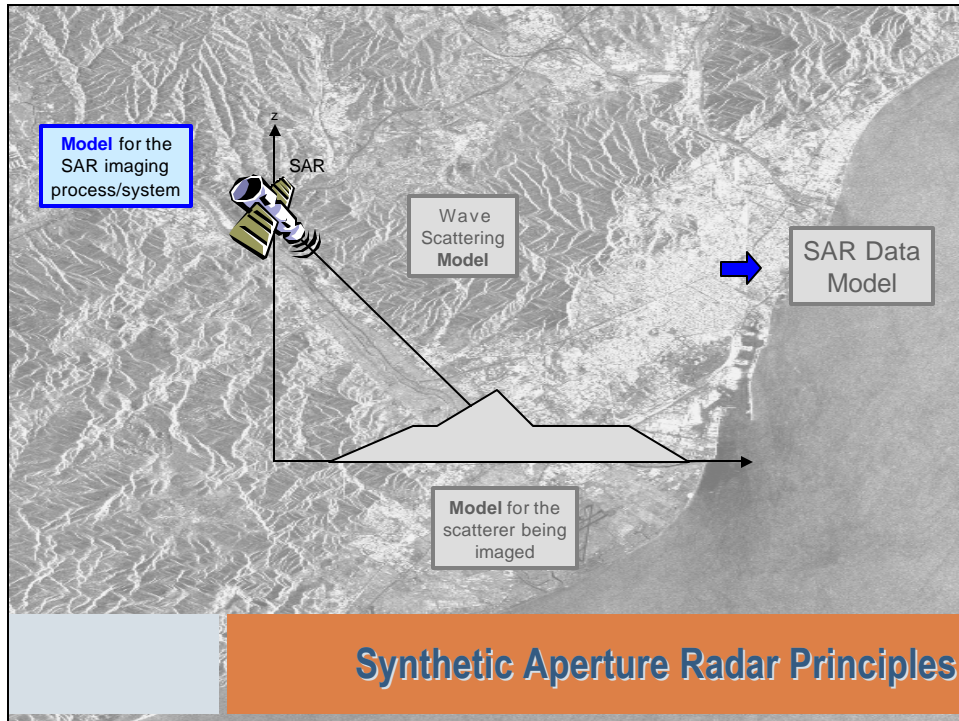


The objective of this tutorial



The analysis and understanding of data acquired by a SAR system needs from the following considerations





## Synthetic Aperture Radar Principles

SAR sensor

$V_{SAR}$

Platform track

Swath

Range

Azimuth

- Side looking geometry
- Two-dimensional imaging system: Range vs. Azimuth
- Different imaging modes. Compromise between resolution and swath coverage
  - Stripmap
  - Scansar
  - Spotlight
- SAR images present a complex nature

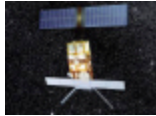
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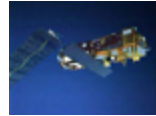




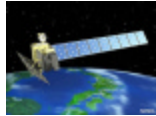
- **Satellite:** Orbital systems



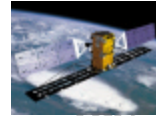
**ERS-1/2**  
ESA (EU)



**ENVISAT / ASAR**  
ESA (EU)



**ALOS / PALSAR**  
NASDA / JAROS (J)



**RADARSAT 2**  
CSA - MDA (CA)



**TERRASAR**  
BMBF / DLR / ASTRIUM

- **Airplane:** Airborne systems



**AIRSAR**  
NASA / JPL (USA)



**ESAR**  
DLR (D)



**PISAR**  
NASDA / CRL (J)



**RAMSES**  
ONERA (F)



**SAR580**  
Environment Canada (CA)

- **Terrestrial platform:** Ground Based SAR system (GB-SAR)



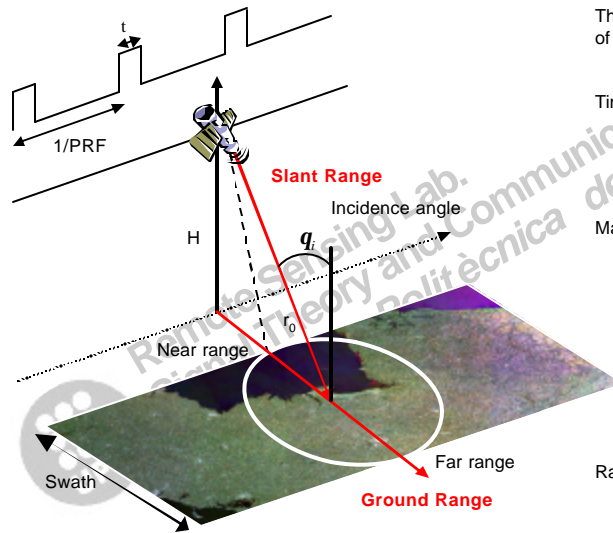
**UPC GB-SAR**  
UPC (SP)



**GBInSAR Lisa**  
LisaLab (I)



In **range** a SAR system operates as a conventional radar



The SAR system transmits pulses of duration  $t$  at PRF frequency

Time delay

$$t_d = \frac{2r_0}{c}$$

Maximum swath

$$SW_{\max} \approx \frac{c}{2 PRF \sin(q_i)}$$

$$q_i \in [20^\circ, 60^\circ]$$

Range resolution

$$d_r = \frac{ct}{2} = \frac{c}{2B}$$



- High spatial resolution, i.e., short transmitted pulses, with sufficient SNR imposes the use of high energy pulses
- ↓
- **Pulse compression** techniques based on modulated long pulses
    - Large radiated energy
    - Range resolution of short pulses
  - Implementation based on **frequency or phase modulation** of the pulse with a bandwidth  $B_{pulse}$ 
    - Chirp pulses
    - In reception, the pulse is processed in a **matched filter** compressing the long pulse to a duration  $1/B_{pulse}$

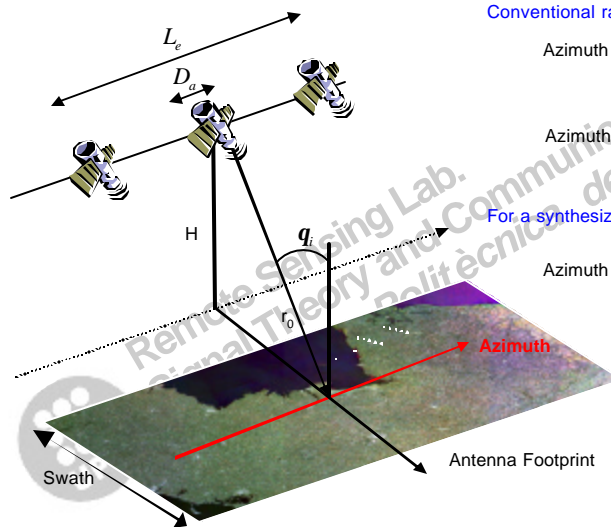


Range resolution

$$d_r = \frac{ct}{2} = \frac{c}{2B_{pulse}}$$



### Difference between SAR system and conventional radars



Conventional radar

$$\text{Azimuth angular spread } q_a \propto \frac{1}{D_a}$$

$$\text{Azimuth resolution } d_a = r_0 q_a = r_0 \frac{1}{D_a}$$

For a synthesized aperture

$$\text{Azimuth angular spread } q_{sa} \propto \frac{1}{2L_c}$$

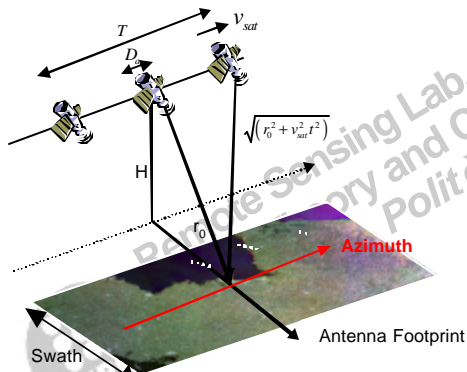
Two-way

$$\text{Azimuth resolution } d_a = r_0 \frac{1}{2L_c}$$

$$L_c < \frac{1R}{D_a} \quad \boxed{d_a > \frac{D_a}{2}}$$



- Azimuth processing is based on the fact that a given target is observed all the time that it is within the antenna footprint. The different observation points are labelled through the **Doppler frequency**

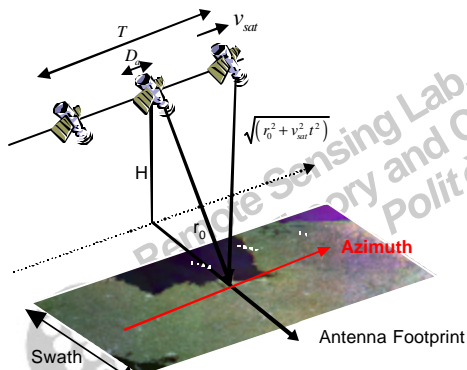


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- Azimuth processing is based on the fact that a given target is observed all the time that it is within the antenna footprint. The different observation points are labelled through the **Doppler frequency**



Doppler frequency definition  $f_{dop} = \frac{1}{2p} \frac{df}{dt}$

Instant phase  $f = f_0 + 2 \frac{2p}{I} \sqrt{(r_0^2 + v_{sat}^2 t^2)}$

Doppler frequency  $f_{dop} = 2 \frac{v_{sat}^2 t}{I r_0}$       $B_{dop} = 2 \frac{v_{sat}^2 T}{I r_0}$

Doppler bandwidth  $T \approx R \frac{I}{L_e} \frac{1}{v_{sat}}$       $B_{dop} \approx 2 \frac{v_{sat}}{D_a}$

Azimuth resolution  $d_a \approx \frac{D_a}{2}$

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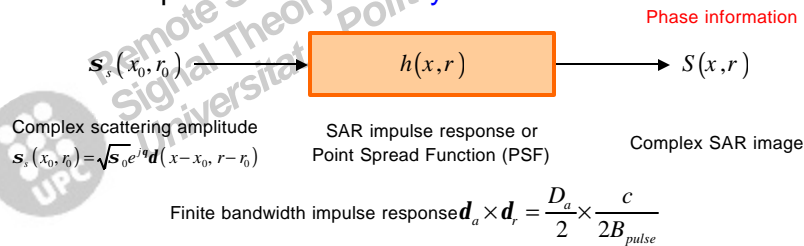
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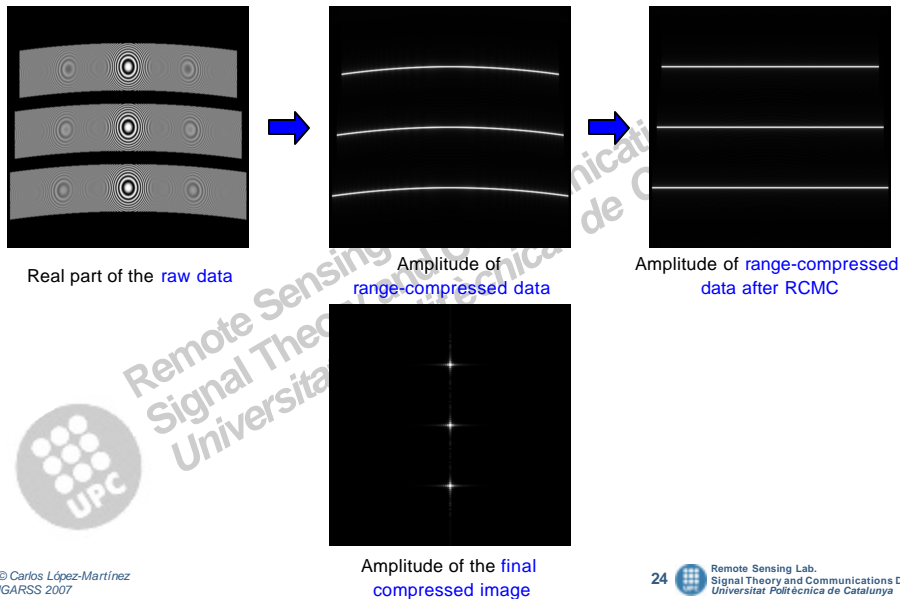
SAR data processing, i.e., SAR image formation process comprises

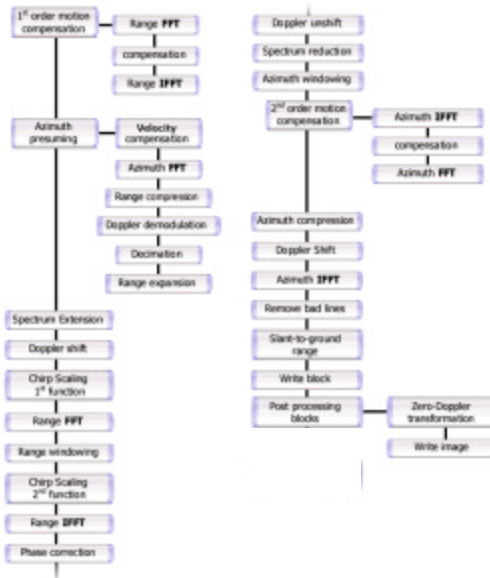
- Data acquisition process
  - Raw data generation. Data recorded by the SAR system
- Image formation process
  - Raw data compression
    - Generation of the synthesized aperture
    - Collecting/Focusing all the contributions of a given target
  - Non-separable/Non-homogeneous bi-dimensional problem

Consider all the process as a **linear system**



**Point scatterer** response focussing process



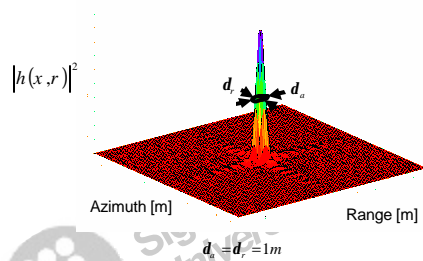


Example of a real processing chain in charge of the image formation process



SAR impulse response function

$$h(x, r) \propto \text{sinc}\left(\frac{px}{d_a}\right) \text{sinc}\left(\frac{pr}{d_r}\right)$$



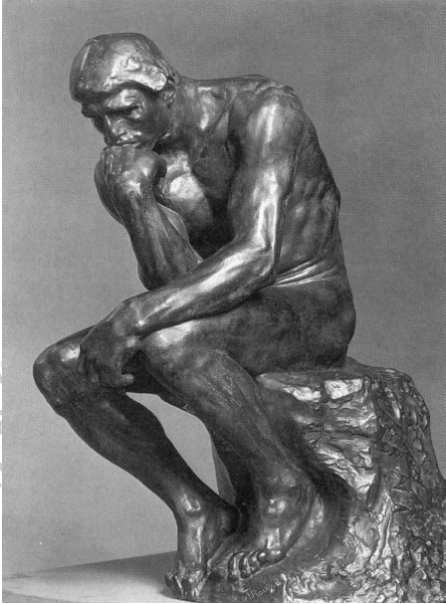
Point scatterer

How it appears in the SAR image  $S(x, r)$

Distributed scatterer

Idea of resolution cell  $d_a \times d_r$

- The resolution cell is not the pixel of the SAR image. The pixel properties depend on how the SAR impulse response is sampled
  - Over sampling induces image spatial correlation



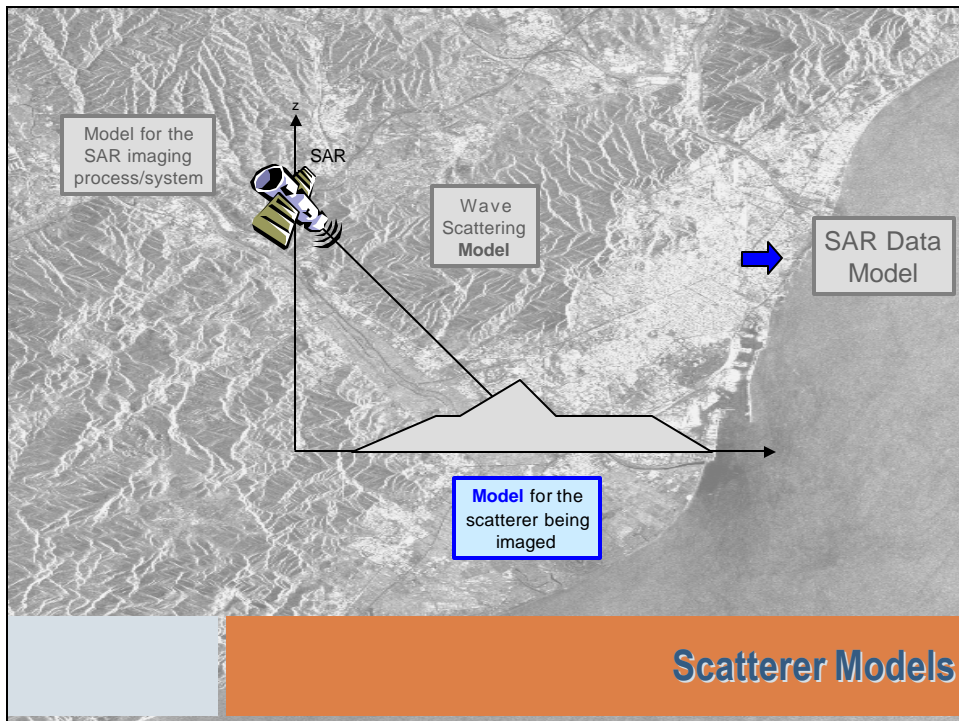
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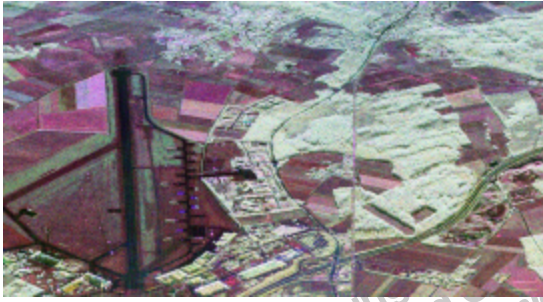
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**Scatterer Models** **Scatterers Heterogeneity**



$|Shh|$   $|Shv|$   $|Svv|$

SAR images reflect the Nature's heterogeneity

L-band (1,3 GHz) fully PolSAR data  
E-SAR system. Oberpfaffenhofen test area (D)




Optical Image  
Oberpfaffenhofen test area (D)

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**Scatterer Models** **Scattering from Point Scatterers**

Examples of point targets imaged by SAR systems



Power lines      Vehicles      Railways      Houses

Types of microwave scattering

- Point scattering
- Complex scattering

Man-made media present a strong point scattering behaviour

↓

Scattered field dominated by canonical scattering mechanisms

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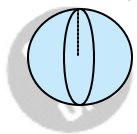
These scatterers make reference to canonical bodies as plates, cylinders, etc...the properties of which can be determined. Each body is finite in extend, and because in the far field zone, the scattered field appears to originated at a point, the body is described as a point target. [Ulaby'90]

$$S_{i,j} = 4p |S_{ij}|^2 \quad i, j = h, v$$

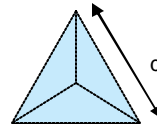
Radar Cross Section or RCS of a body. Scattered power as a function of the incident power. Depends on the imaging geometry

$$S_s(x_0, r_0) = \sqrt{s} e^{j\alpha} d(x-x_0, r-r_0)$$

Object description (Deterministic description)



$$S_{\max}(m^2) = pd^2$$



$$S_{\max}(m^2) = \frac{4pd^4}{3l^2}$$



Examples of natural targets imaged by SAR systems



Rocks



Rough surface



Snow



Sea ice



Vegetation cover

Types of microwave scattering

- Surface scattering
- Volume scattering

Geophysical media present complicate structures and/or compositions



Exact knowledge of the scattered field very difficult





Radar scattering from terrain involves complicated interactions because the scattering elements have complicated geometries and are randomly distributed in space. (...) Hence, we usually focus our attention on the development of generic models that can help to understand the nature of wave propagation and scattering in random media (...) allowing to interpret radar observations and extract useful information. [Ulaby'90]

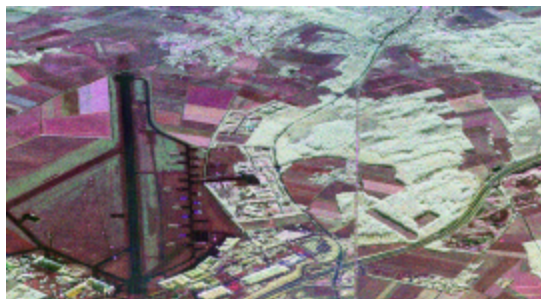
$u(\vec{r})$  Object scattering function. (Random function - microscopic structure) NOT ACCESSIBLE  
Distributed scatterers have complex geometries and are randomly distributed

$\langle u(\vec{r}) \cdot u(\vec{r}') \rangle = \mathbf{s}^0 \cdot \mathbf{d}(\vec{r} - \vec{r}')$  Object description. (2<sup>nd</sup> order descriptor - macroscopic structure)



$$\mathbf{s}^0 = E \left\{ \frac{\mathbf{S}}{A} \right\}$$

Average scattering coefficient or Differential backscattering coefficient. Does not depend on the area of the cell of resolution. This normalisation is necessary as a distributed target can occupy more than one cell of resolution.



|Shh| |Shv| |Svv|



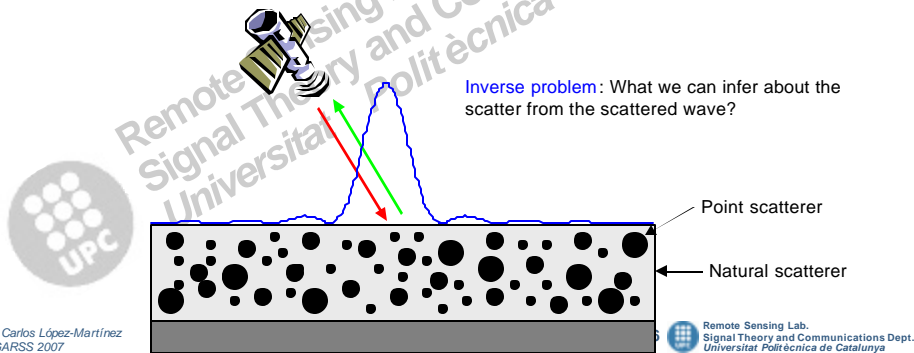
L-band (1.3 GHz) fully PolSAR data  
E-SAR system. Oberpfaffenhofen test area (D)

- **Homogeneous areas:** Zones characterized for presenting a constant behaviour, i.e., a stationary mean value
- **Non-Homogeneous areas:** Zones presenting the same natural characteristics (forest, grass, etc...) but characterized by non-stationary properties
  - Data texture
- Data texture is subjected to the notion of **information scale**



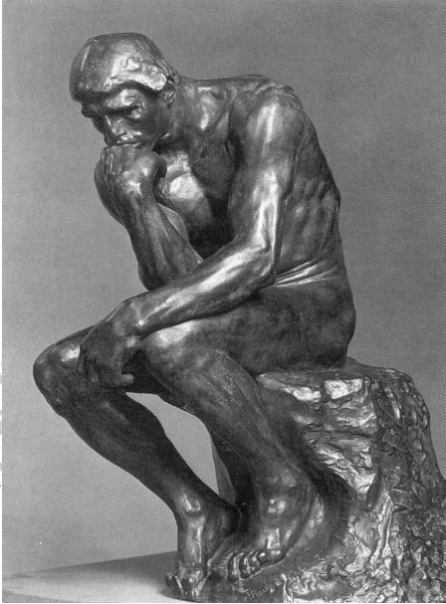
**Real scatterers** present very complex structure

- Consider real scatterers as a collection of point or individual scatterers, randomly located
- The internal structure, i.e., microscopic structure, of the scatterer covered by the resolution cell can non be resolved
  - Partially solved by high dimensional SAR systems (PolInSAR)
- Scattered field results from the interaction of the incident wave with the individual scatterers



Types of complex scatterers

- **Surface** scatterer
  - The scattered wave is produced on the surface of the scatterer (Conducting or homogeneous media)
  - The surface is considered as a set of facets. Discrete surface
- **Volume** scatterer
  - The scattered wave is produced within the scatterer (Inhomogeneous media)
- **Point** scatterer
  - The scattered wave is mainly produced by a dominant point scatterer



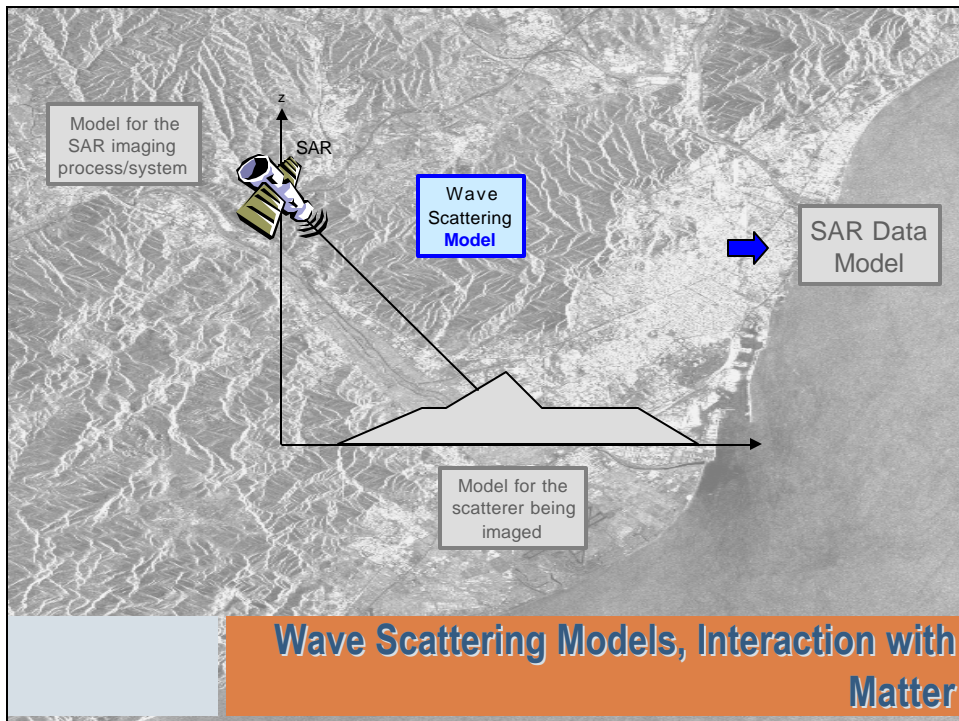
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The response of a point scatterer, i.e., how it appears in a SAR image, can be considered as **deterministic**

$$s_s(x_0, r_0) = \sqrt{S} e^{j\theta} d(x - x_0, r - r_0) \quad h(x, r) \propto \text{sinc}\left(\frac{px}{d_a}\right) \text{sinc}\left(\frac{pr}{d_r}\right)$$

$$S(x, r) = s_s(x_0, r_0) ** h(x, r) \quad \text{Convolution in the Range-Azimuth space}$$



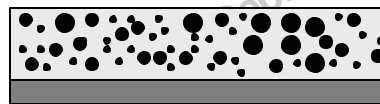
$$S(x, r) \propto s_s(x_0, r_0) \exp\left(j2\frac{2p}{l}(r - r_0)\right) \text{sinc}\left(\frac{p(x - x_0)}{d_a}\right) \text{sinc}\left(\frac{p(r - r_0)}{d_r}\right) \quad \text{Complex SAR image}$$

- Given the SAR image, it is possible to determine the properties of the scatterer from the image itself
- The pixel contains all the necessary information to characterize the scatterer



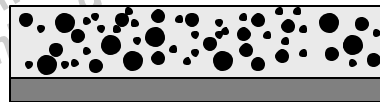
The **complexity** of a distributed scatterer is translated to the **scattering process** in the scatterer

Given a set of resolution cells/pixels, the internal structure (microscopic structure) changes from pixel to pixel, then, the scattering process changes from pixel to pixel



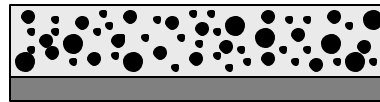
Pixel 1

• Scattering processes can not be characterized by the value of single pixels as its values depend on the internal random arrangement



Pixel 2

• Scattering processes must be characterized by global parameters common to all the pixels



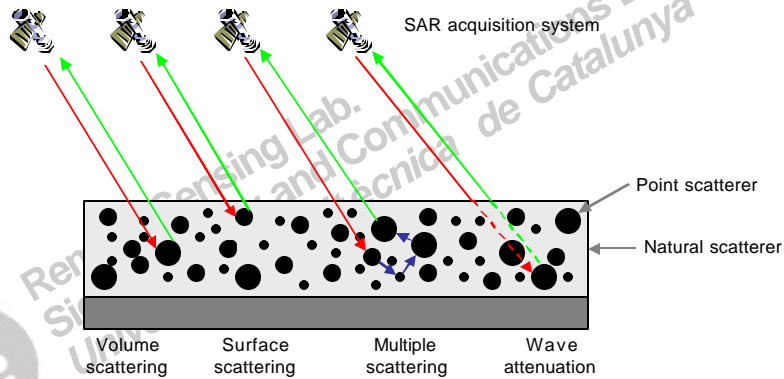
Pixel 3

Characterization based on Statistical parameters



Scattering based on the **Born approximation** or **single scattering approximation**

- The scattering is supposed to be the **linear** coherent addition of the individual scattered waves from a set of discrete or point scatterers



- The model does not consider **attenuation** or **multiple scattering**



Real **three dimensional** scenes are translated to a **two dimensional** SAR image

- SAR system **impulse response**

$$h(x, r) \propto \text{sinc}\left(\frac{px}{d_a}\right) \text{sinc}\left(\frac{pr}{d_r}\right)$$

- Scatterer **model**

- Complex reflectivity function, Object scattering function
- Random nature
- Describes the reflectivity of each point scatterer

$$u(\vec{r}) = u(x, y, z)$$

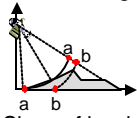
- The complex reflectivity function must be transformed into a two-dimensional function. Introduction of image distortions

$$u(x, r) = \int u(x, y_0 + r \sin \mathbf{q}, z_0 - r \cos \mathbf{q}) r d\mathbf{q}$$

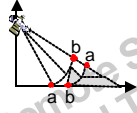


The side-looking geometry and the two-dimensional nature of the SAR images introduce **image distortions**

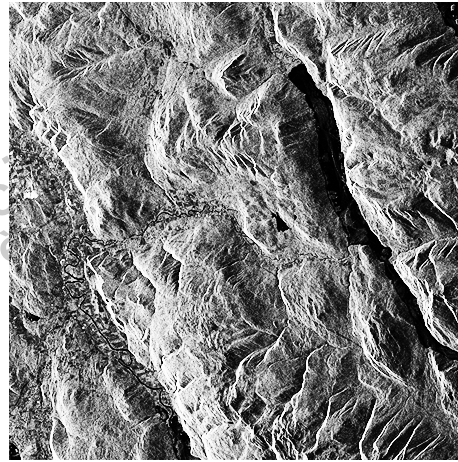
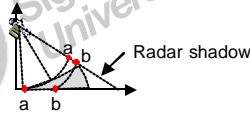
- **Foreshortening**. Slope of local terrain is less than incidence angle



- **Layover**. Slope of local terrain is higher than incidence angle



- **Shadowing**. Magnitude of negative slopes is greater than incidence angle

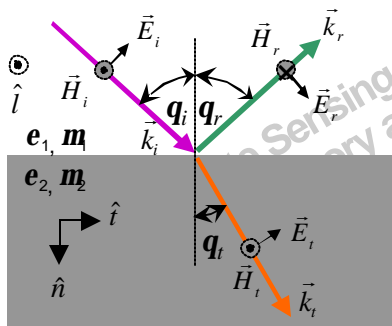


ERS 1 Image



**Reflected waves**, coming from surface scattering, appear on the surface plane dividing two semi-infinite **homogeneous media**

- Oblique incidence in lossless media where **E-field is parallel to the plane of incidence**



Incident electric field

$$\vec{E}_i = [\hat{t} \cos q_i - \hat{n} \sin q_i] E_0 e^{-j b_1 [t \sin q_i + n \cos q_i]}$$

Reflected electric field

$$\vec{E}_r = [\hat{t} \cos q_r + \hat{n} \sin q_r] E_0 \Gamma_{\parallel}^b e^{-j b_1 [t \sin q_r - n \cos q_r]}$$

Transmitted electric field

$$\vec{E}_t = [\hat{t} \cos q_t - \hat{n} \sin q_t] E_0 T_{\parallel}^b e^{-j b_2 [t \sin q_t + n \cos q_t]}$$

Transmission and reflection coefficients

$$\Gamma_{\parallel}^b = [h_2 \cos q_i - h_1 \cos q_i] / [h_2 \cos q_i + h_1 \cos q_i]$$

$$T_{\parallel}^b = 2 h_2 \cos q_i / [h_2 \cos q_i + h_1 \cos q_i]$$

**Wave Scattering Models** **Surface Scattering**

- Oblique incidence in lossless media where E-field is perpendicular to the plane of incidence

Incident electric field

$$\vec{E}_i = \hat{l} E_0 e^{-j\mathbf{b}_1[\sin q_i + n \cos q_i]}$$

Reflected electric field

$$\vec{E}_r = \hat{l} E_0 \Gamma_{\perp}^b e^{-j\mathbf{b}_1[\sin q_r - n \cos q_r]}$$

Transmitted electric field

$$\vec{E}_t = \hat{l} E_0 T_{\perp}^b e^{-j\mathbf{b}_2[\sin q_t + n \cos q_t]}$$

Transmission and reflection coefficients

$$\Gamma_{\perp}^b = \frac{h_2 \cos q_i - h_1 \cos q_t}{h_2 \cos q_i + h_1 \cos q_t}$$

$$T_{\perp}^b = \frac{2h_2 \cos q_i}{h_2 \cos q_i + h_1 \cos q_t}$$

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**Wave Scattering Models** **Surface Scattering**

RCS ( $s^0$ ) of surfaces depends on

- Roughness
  -
- Dielectric permittivity, related with the water content
  - Humidity  $\uparrow \Rightarrow S^0 \uparrow$
- Roughness and humidity are coupled parameters in SAR measurements

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Volume scattering appears in **non-homogeneous** media. The capacity to produce volume scattering depends on the penetration depth

The penetration depth  $dp$  corresponds to the distance in which the energy is attenuated a factor equal to  $1/e$

Propagation constant

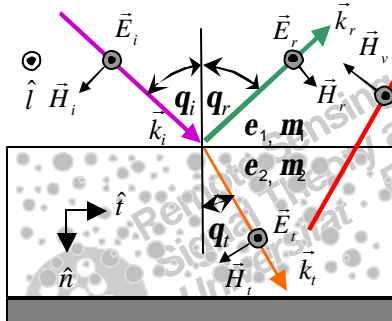
$$k = \frac{2\pi}{\lambda} = k_0 \sqrt{\epsilon_r} = a + jb \quad b \geq 0$$

Transmitted field

$$\vec{E}_t = \vec{E}_0 e^{jaz} e^{-bz}$$

Penetration depth (field attenuation  $1/\sqrt{e}$ )

$$dp = \frac{1}{2b} = \frac{1}{2k_0 \Im\{\sqrt{\epsilon_r}\}} \propto l$$

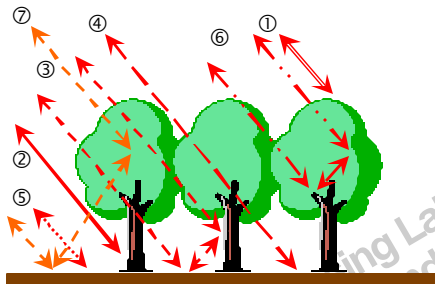


Wavelength ↗ ⇒  $dp$  ↗

Frequency ↗ ⇒  $dp$  ↘



Main scattering mechanism in **forest**



1.Canopy scattering

2.Trunk scattering

3.Trunk-soil interaction

4.Attenuated soil scattering

5.Direct soil scattering

6.Trunk-branches scattering

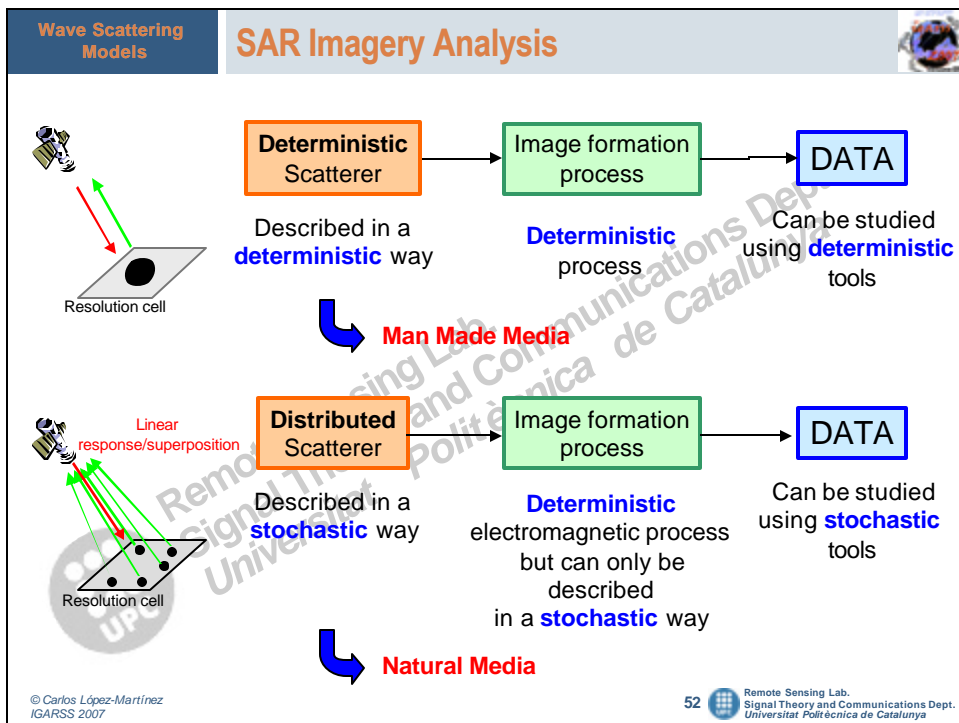
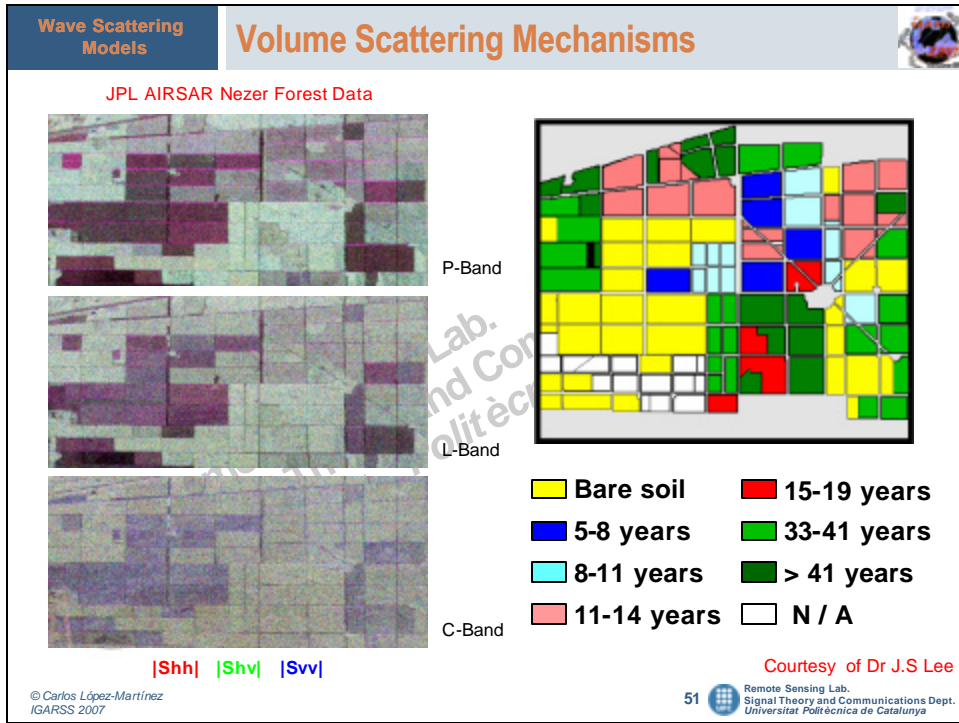
7.Branches -soil interaction

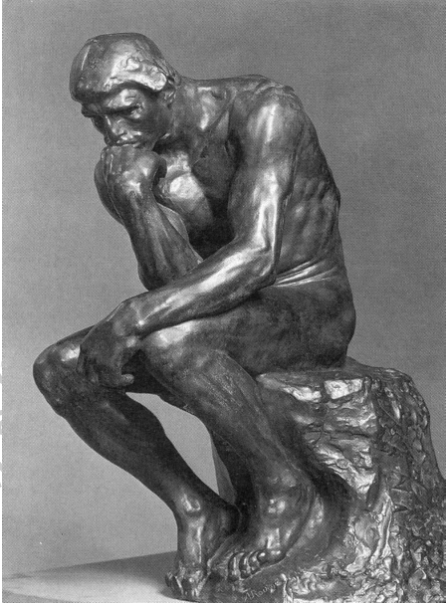
Biomass ↗ ⇒  $s^0$  ↗

Frequency ↗ ⇒ Penetration ↘

Volume scattering composed by complex scattering mechanisms. Born approximation is no longer valid



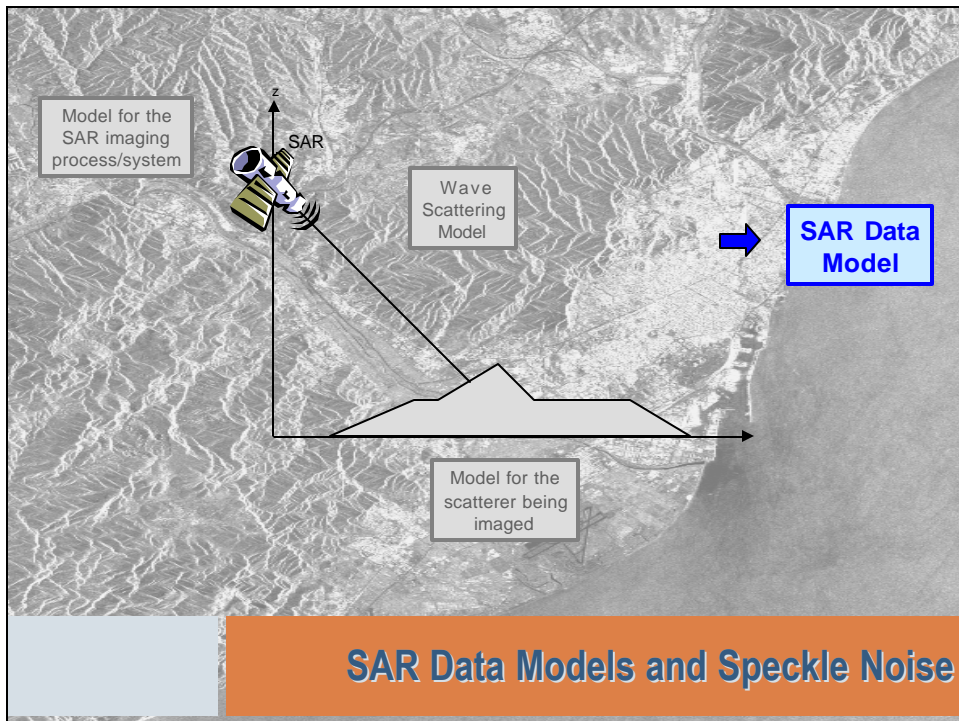




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Speckle corresponds to the  
“Salt&Pepper” effect of the image



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|Svv|

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On the basis of the discrete scatterer description

$$S(x, r) = \int_{-\infty-\infty}^{\infty} \int_{-\infty-\infty}^{\infty} u(x', r') h(x-x', r-r') dx' dr' \quad \Rightarrow \quad S(x, r) = \frac{1}{\sqrt{L}} \sum_{k=1}^L \sqrt{S_k} e^{j\phi_k} h(x-x_k, r-r_k)$$

↓  
 Normalizing factor

L: Number of point scatterers embraced by the resolution cell

- L as a **deterministic** quantity
  - L = 1: or a dominating point scatterer: Deterministic scattering
    - Rice/Rician model
  - L > 1: Partially developed speckle
    - Not solved model. Even numerical solution difficult
  - L >> 1: Fully developed speckle
    - Gaussian model
- L as a **stochastic** quantity
  - L characterized by a pdf: Image texture
    - K-distribution model

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- SAR image formation process

$$S(x, r) = \frac{1}{\sqrt{L}} \sum_{k=1}^L \sqrt{s_k} e^{j\theta_k} h(x - x_k, r - r_k)$$

- Complex SAR data for  $L \gg 1$

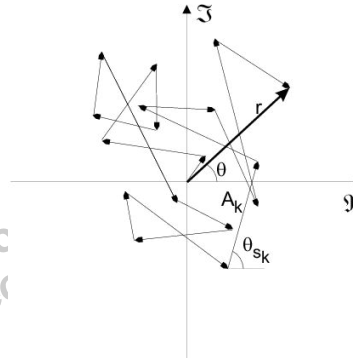
$$S(r(x, r), \mathbf{q}(x, r)) = \Re\{S\} + j\Im\{S\} = r(x, r) \exp(j\mathbf{q}(x, r))$$

- Real part

$$\Re\{S\} = \frac{1}{\sqrt{L}} \sum_{k=1}^L A_k \cos(\mathbf{q}_{s_k})$$

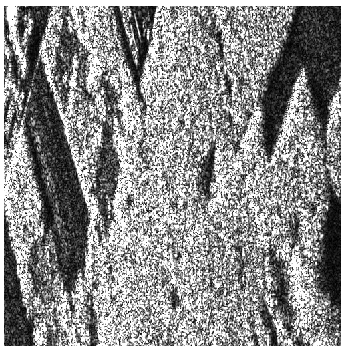
- Imaginary part

$$\Im\{S\} = \frac{1}{\sqrt{L}} \sum_{k=1}^L A_k \sin(\mathbf{q}_{s_k})$$



Random Walk Process

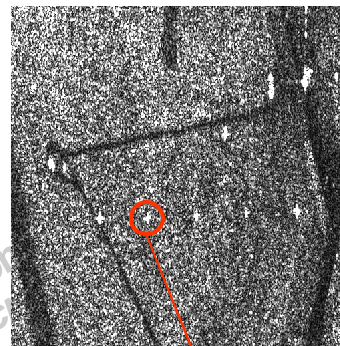
$$r(x, r) \exp(j\mathbf{q}(x, r)) = \frac{1}{\sqrt{L}} \sum_{k=1}^L A_k \exp(j\mathbf{q}_{s_k})$$



Fully Developed speckle

Bright points: Points where the interference is **constructive**

Dark points: Points where the interference is **destructive**



Corner reflector  
Dominant scatterer  
**No speckle**

**Speckle is the interference or fading pattern**

**S<sub>0</sub> amplitude**  
E-SAR L-band system



- **Completely developed Speckle** (large L and no dominant scatterer)
  - Hypotheses
    - The amplitude  $A_k$  and the phase  $q_k$  of the  $k$ th scattered wave are statistically independent of each other and from the amplitudes and phases of all other elementary waves (Uncorrelated point scatterers)
    - The phases of the elementary contributions  $q_k$  are equally likely to lie anywhere in the primary interval  $[-p, p]$
- **Central Limit Theorem**  $S = \mathcal{N}_{c^2}(0, \mathbf{s}^2/2)$ 
  - Real Part  $\left. \begin{array}{l} \text{Gaussian Model} \\ \text{Gaussian Hypothesis} \end{array} \right\}$ 

$$p_{\Re\{S\}}(\Re\{S\}) = \frac{1}{\sqrt{2p\mathbf{s}^2}} \exp\left(-\frac{1}{2}\left(\frac{\Re\{S\}}{\mathbf{s}}\right)^2\right) \quad \Re\{S\} \in (-\infty, \infty) \quad \text{Gaussian pdf}$$
  - Imaginary Part
 
$$p_{\Im\{S\}}(\Im\{S\}) = \frac{1}{\sqrt{2p\mathbf{s}^2}} \exp\left(-\frac{1}{2}\left(\frac{\Im\{S\}}{\mathbf{s}}\right)^2\right) \quad \Im\{S\} \in (-\infty, \infty) \quad \text{Gaussian pdf}$$
  - Real and imaginary parts are uncorrelated  $E\{\Re\{S\}\Im\{S\}\} = 0$



- Amplitude: Rayleigh pdf
 
$$p_r(r) = \frac{r}{\mathbf{s}^2} \exp\left(-\frac{1}{2}\left(\frac{r}{\mathbf{s}}\right)^2\right) \quad r \in [0, \infty)$$

$$E\{r\} = \sqrt{\frac{p}{2}}\mathbf{s}$$

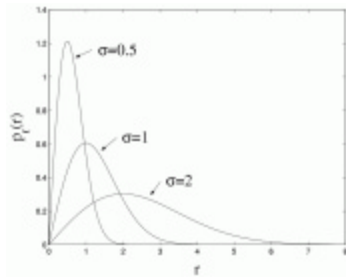
$$E\{r^2\} = 2\mathbf{s}^2$$

$$\mathbf{s}_r^2 = E\{r^2\} - E^2\{r\} = \left(2 - \frac{p}{2}\right)\mathbf{s}^2$$
- Intensity ( $I=r^2$ ): Exponential pdf
 
$$p_I(I) = \frac{1}{2\mathbf{s}^2} \exp\left(-\frac{I}{2\mathbf{s}^2}\right) \quad I \in [0, \infty)$$

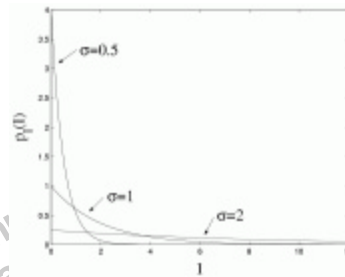
$$E\{I\} = 2\mathbf{s}^2 \equiv \mathbf{s}$$

$$E\{I^2\} = 2(2\mathbf{s}^2)^2$$

$$\mathbf{s}_I^2 = E\{I^2\} - E^2\{I\} = (2\mathbf{s}^2)^2$$
- Phase: Uniform pdf. Contains NO information
 
$$p_q(q) = \frac{1}{2p} \quad q \in [-p, p]$$
- Amplitude and phase are uncorrelated



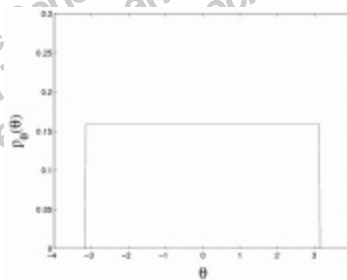
Amplitude: Rayleigh pdf



Intensity ( $I=r^2$ ): Exponential pdf



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Phase: Uniform pdf



### Important considerations

- Speckle is a **deterministic** electromagnetic effect, but due to the complexity of the image formation process, it must be analysed **statistically**
- Considering completely developed speckle, a SAR image pixel does not give information about the target. Only statistical moments can describe the target or the process



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What does it mean **information** in the presence of Speckle?

- Phase contains no information
- Intensity exponentially distributed

$$p_I(I) = \frac{1}{2s^2} \exp\left(-\frac{I}{2s^2}\right) \quad I \in [0, \infty)$$

Exponential pdf



$$\begin{aligned} E\{I\} &= 2s^2 \\ s_I &= 2s^2 \end{aligned}$$

First and second order moments

- Intensity, under the previous hypotheses, is completely determined by the exponential pdf
  - Pdf completely determined by the pdf shape
  - Pdf shape parameterized by  $s$  → **INFORMATION** →  $RCS s^0$
- Not useful information is considered as **NOISE**



Objectives of a **Noise Model**

- To embed the data distribution into a noise model, that is, a function that allows identifying of the useful information to be retrieved, the noise sources, and how these terms interact
- Optimize the information extraction process, i.e., the noise filtering process

SAR image intensity noise model

$$\text{SAR image intensity } (I=r^2) \quad p_I(I) = \frac{1}{2s^2} \exp\left(-\frac{I}{2s^2}\right) \quad I \in [0, \infty) \quad \begin{aligned} E\{I\} &= 2s^2 \\ s_I &= 2s^2 \end{aligned}$$

$$I = 2s^2 n$$

$$p_n(n) = \exp(-n) \quad n \in [0, \infty)$$

$$\begin{aligned} E\{I\} &= 1 \\ s_I &= 1 \end{aligned}$$

One dimensional speckle noise model (Model over the SAR image intensity - 2<sup>nd</sup> moment)



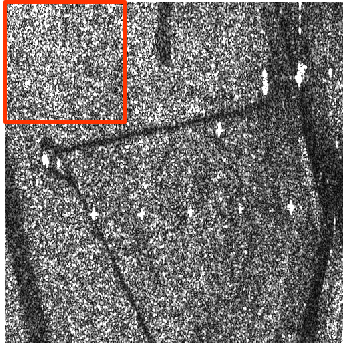
$$I(x, r) = s(x, r) n(x, r)$$

**Multiplicative Speckle Noise Model**

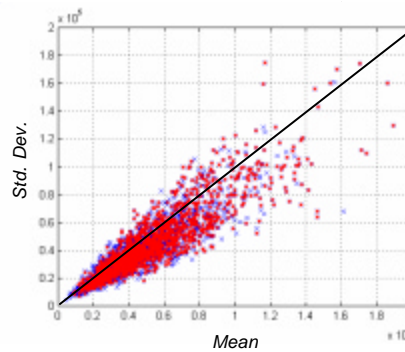


Moments calculated over local 7x7 local windows

Statistics area



Grass area



Blue:  $|S_{hh}|^2$   
Red:  $|S_{vv}|^2$



$S_{hh}$  amplitude  
E-SAR L-band system



Analysis of the Coefficient of Variation CV

$$CV = \frac{std}{mean}$$

$$E\{I\} = 2s^2 \quad s_I = 2s^2 \quad CV = \frac{std}{mean} = \frac{2s^2}{2s^2} = 1$$

For the exponential PDF CV=1

- An increase of the power transmitted by the SAR system does not produce an increase of the Signal to Noise Ratio (SNR)

Analysis of the Equivalent Number of Looks (ENL)

$$ENL = CV^{-1} = \frac{mean}{std}$$







## Statistical Product Model

- Intensity is decomposed into a three term product

$$I(x, r) = s(x, r) T(x, r) n(x, r)$$

$s$  : Mean value

$T$  : Texture random variable

$n$  : Fading random variable (speckle)

## Three scale model

- Coarsest scale : Mean reflectivity, constant value
- Finest scale : Speckle, noise
- Intermediate scale : Texture, spatially correlated fluctuations

As observed, the definition of the three terms is subjected to the notion of scale, or in other words, to where limits between them are placed

- Analysis based in time/frequency tools



## How to describe texture in SAR images

- One-point statistics: Mean and Variance
  - K-distribution model
- Two-point statistics: Autocovariance, Autocorrelation function (ACF)
  - Modelization of the autocovariance and autocorrelation functions





- Texture can be considered as a **fluctuating mean value**

$$I(x, r) = \mathbf{s}(x, r)T(x, r)n(x, r)$$

$$p_I(I) = \frac{1}{2\mathbf{s}^2} \exp\left(-\frac{I}{2\mathbf{s}^2}\right) \quad I \in [0, \infty) \quad \Rightarrow \quad p_I(I) = \frac{I}{\mathbf{s}} \exp\left(-\frac{I}{\mathbf{s}}\right) \quad I \in [0, \infty)$$

Simplification

$$P(I) = \int_0^\infty P(I|\mathbf{s})P(\mathbf{s})d\mathbf{s} = \frac{L^L I^{L-1}}{\Gamma(L)} \int_0^\infty \frac{d\mathbf{s}}{\mathbf{s}^L} \exp\left[-\frac{LI}{\mathbf{s}}\right] P(\mathbf{s})$$

Gaussian PDF

Fluctuating RCS

- Model results from considering the number of scatterers L within the resolution cell as a **random quantity**



RCS model  $\Rightarrow$  Gamma pdf  $P(\mathbf{s}) = \left(\frac{v}{\langle \mathbf{s} \rangle}\right)^v \frac{\mathbf{s}^{v-1}}{\Gamma(v)} \exp\left[-\frac{v\mathbf{s}}{\langle \mathbf{s} \rangle}\right]$

$v$  : Order parameter

$\langle \mathbf{s} \rangle$ : Mean RCS  $\mathbf{s}(x, r)$

Number of scatterers controlled by a **bird, death and migration process**, the population would be **negative binomial**



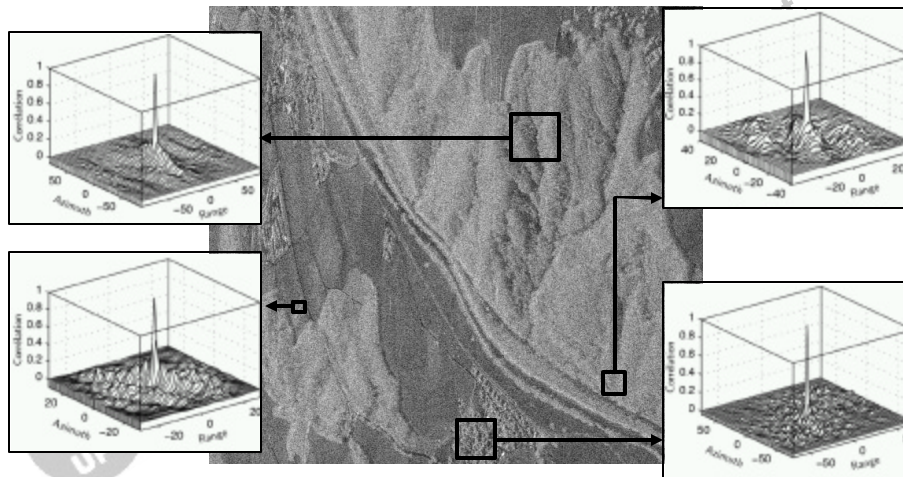
$$P(I) = \frac{2}{\Gamma(L)\Gamma(v)} \left(\frac{Lv}{\langle I \rangle}\right)^{(L+v)/2} I^{(L+v-2)/2} K_{v-L} \left[ 2 \left(\frac{vLI}{\langle I \rangle}\right)^{1/2} \right]$$

Intensity distributed as K-distribution



Texture can be considered as a fluctuating autocovariance function

Trautstein, ESAR, DLR, L-Band



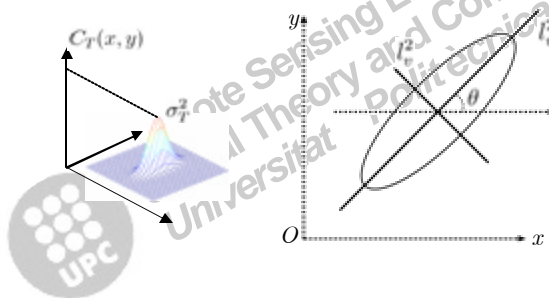
Nonstationary texture  
Anisotropic texture



Modelling of the local autocovariance function considering Anisotropic Gaussian Kernels AGK

- Consider that locally, the autocovariance function can be approximated by an orientated two-dimensional Gaussian function

$$C_T(\mathbf{d}) = \sigma_T^2 \exp(-\mathbf{d}^T \Sigma^{-1} \mathbf{d}) \quad \mathbf{d} = [x, y]^T$$



$$\Sigma = \mathbf{R}_\theta^T \Lambda \mathbf{R}_\theta$$

Correlation lengths

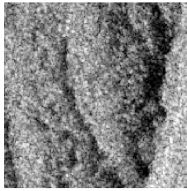
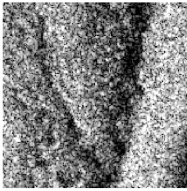
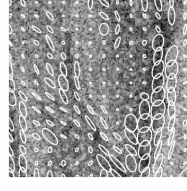
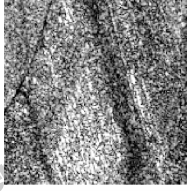
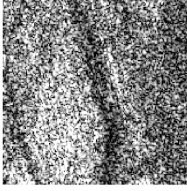
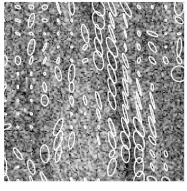
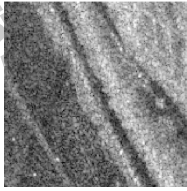
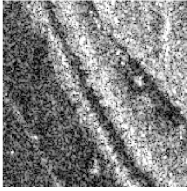
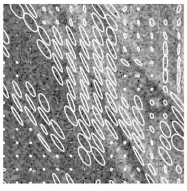
$$\Lambda = \begin{bmatrix} l_u^2 & 0 \\ 0 & l_v^2 \end{bmatrix}$$

Orientation Angle

$$\mathbf{R}_\theta = \begin{bmatrix} \cos \theta & -\sin \theta \\ \sin \theta & \cos \theta \end{bmatrix}$$

SAR Data Models and Speckle Noise

## Two-Point Statistics Texture

	SPAN	$ S_{hh} $	
Zone 1			
Zone 2			
Zone 3			

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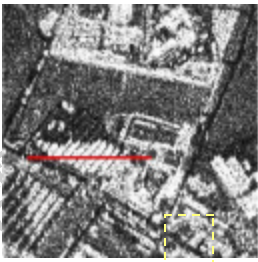
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SAR Data Models and Speckle Noise

## Speckle Noise Model

### Observation

- The Gaussian statistical model is unable to accommodate larger tails, i.e., a higher probability of larger SAR images amplitudes



↓

Gaussian statistics must be **extended**

↓

Consider a **family of distributions** in which the Gaussian distribution is a member

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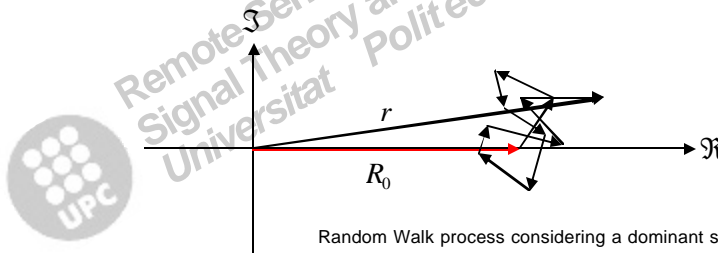


- SAR image formation process

$$S(x, r) = \frac{1}{\sqrt{L}} \sum_{k=1}^L \sqrt{s_k} e^{jq_k} h(x - x_k, r - r_k)$$

- Now consider that within the resolution cell there is a **dominant point scatterer**

$$S(x, r) = R_0 + \frac{1}{\sqrt{L}} \sum_{k=1}^L \sqrt{s_k} e^{jq_k} h(x - x_k, r - r_k)$$



Under the same assumptions for **fully developed speckle**, but considering the contribution of the dominant point scatterer

- Real and Imaginary Parts

$$P_{\Re\{S\}, \Im\{S\}}(\Re\{S\}, \Im\{S\}) = \frac{1}{2\pi s^2} \exp\left(-\frac{(\Re\{S\} - R_0)^2 + \Im^2\{S\}}{2s^2}\right)$$

- Amplitude: Rician pdf

$$P_r(r) = \frac{r}{s^2} \exp\left(-\frac{r^2 + R_0^2}{2s^2}\right) I_0\left(\frac{rR_0}{s^2}\right) \quad I_0(x) \text{ Bessel function of first kind, order zero}$$

$$E\{r\} = \frac{1}{2} \sqrt{\frac{P}{2s^2}} \exp\left(-\frac{R_0^2}{4s^2}\right) \left[ (R_0^2 + 2s^2) I_0\left(\frac{R_0^2}{4s^2}\right) + R_0^2 I_1\left(\frac{R_0^2}{4s^2}\right) \right]$$

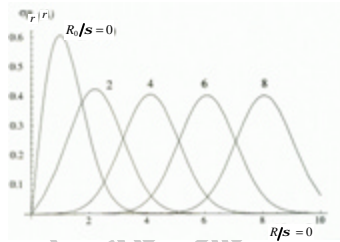
$$E\{r^2\} = R_0^2 - 2s^2$$



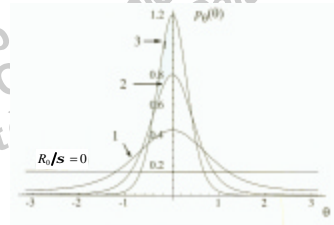
- Phase

$$p_q(\mathbf{q}) = \frac{e^{-\frac{R_0^2}{2s^2}}}{2p} + \sqrt{\frac{1}{2p}} \frac{R_0}{s} e^{-\frac{R_0^2}{2s^2} \sin^2 q} \frac{1 + \operatorname{erf}\left(\frac{R_0 \cos q}{\sqrt{2s}}\right)}{2} \cos q$$

- Examples of pdfs



Amplitude pdf

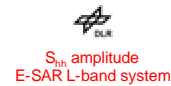


Phase pdf

- SAR image example



Corners reflectors

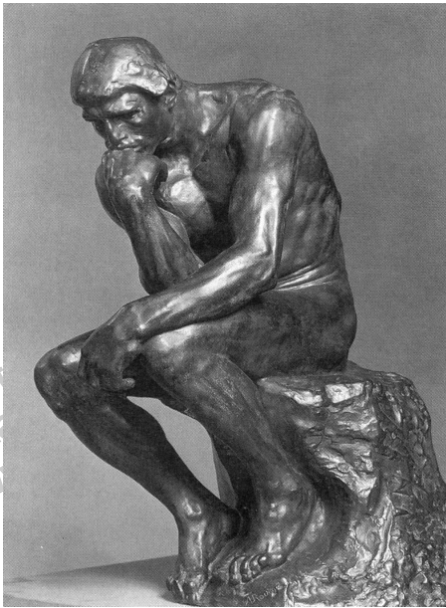


In extremely heterogeneous areas the Gaussian distribution is unable to predict the data distribution

- The solution is to consider more complex distributions with a larger number of parameters
- Difficulty to estimate these parameters with a reduced number of samples
- These models tend to model the pair Texture/Speckle and not only Speckle. No differences are established between point and distributed scatterers

$$I(x, r) = S(x, r)T(x, r)n(x, r)$$

- Extremely heterogeneous areas correspond mainly to urban areas



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**Multidimensional SAR Systems**



- SAR Interferometry (InSAR):  $m=2$ . Topographic information
- Differential SAR interferometry (DInSAR):  $m=3$ . Topographic changes information
- SAR Polarimetry (PolSAR):  $m=3,4$ . Geometric characterization and classification of the scatterers being imaged
- Polarimetric SAR interferometry (PolInSAR):  $m=6,8$ . Study and characterization of volumetric structures
- SAR Tomography/Multibaseline:  $m>2$ . Vertical profiling
- Multitemporal SAR:  $m>2$ . Change detection and temporal analysis
- Multifrequency SAR:  $m>2$ . Characterization of the scatterers being imaged



Important aspects to consider in Multidimensional SAR Imagery

- Physics
  - Depending on the configuration of the multidimensional SAR system, information is sensitive to one or several properties of the target being imaged
  - Data processing, and specially, data estimation can not be done without taking into account the physics behind the scattering process
  - The most clear example is the number of channels  $m$ . Represents a clear limitation for multidimensional SAR imagery
- Mathematical representation, Statistics
  - A mathematical description is necessary to systemize data description and understanding

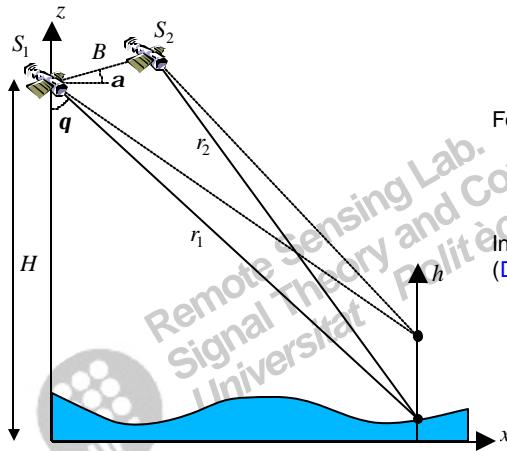


Electromagnetic Signal Processing





Spatial diversity makes SAR data sensitive to **terrain topography**



Coherent information

$$S_1 = r_1 e^{j\phi_1} = r_1 e^{j\left(\frac{4\pi}{\lambda} r_1 + \phi_{obj1}\right)}$$

$$S_2 = r_2 e^{j\phi_2} = r_2 e^{j\left(\frac{4\pi}{\lambda} r_2 + \phi_{obj2}\right)}$$

For small baselines

$$r_1 \approx r_2$$

$$\phi_{obj1} \approx \phi_{obj2}$$

Interferometric phase difference  
(Deterministic phase component)

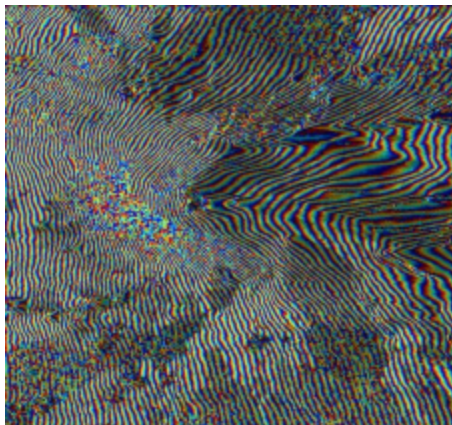
$$\Delta\phi_{12} = \text{Arg}(S_1 S_2^*) = \frac{4\pi}{\lambda} \Delta r_{12}$$

$\Delta r_{12}$  can be estimated with a  
sub-wavelength accuracy

**High accuracy estimation of h**

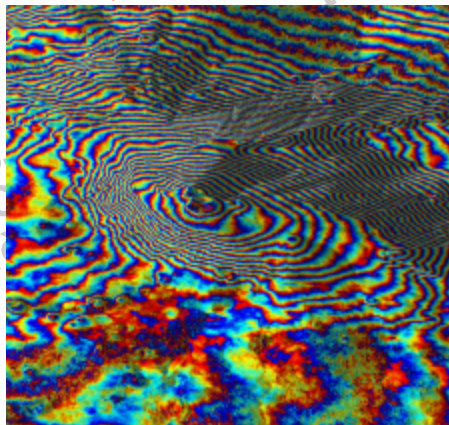


SIR-C, X-band, Mount Etna / Italy



$$\Delta\phi_{12} = \Delta\phi_{topo} + \Delta\phi_{fe}$$

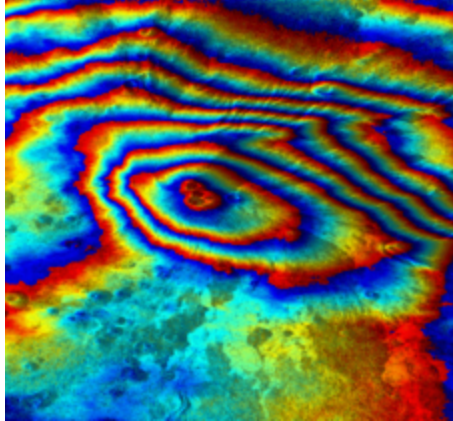
60m baseline



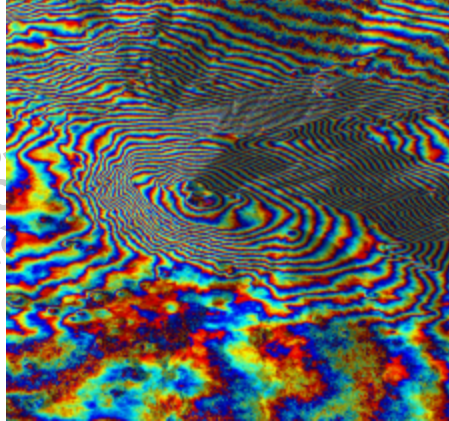
$$\Delta\phi_{12} - \Delta\phi_{fe} = \Delta\phi_{topo}$$



SIR-C, X-band, Mount Etna / Italy



Simulated 12m baseline



60m baseline

$$\Delta f_{topo} = \frac{4p}{l} \frac{B_{\perp}}{r_1 \sin q} \Delta h$$

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### Interferometric coherence

- Joint interferometric representation

$$\mathbf{k} = \begin{bmatrix} S_1 \\ S_2 \end{bmatrix} \text{ is } S = \mathcal{N}_{c^2}(0, \mathbf{C}_k)$$

$$\text{with } \mathbf{C}_k = E\{\mathbf{k}\mathbf{k}^H\} = \begin{bmatrix} \bar{I}_1 & \mathbf{r}\sqrt{\bar{I}_1\bar{I}_2} \\ \mathbf{r}^*\sqrt{\bar{I}_1\bar{I}_2} & \bar{I}_2 \end{bmatrix} \text{ and } \bar{I}_i = E\{S_i S_i^H\}$$

- Interferometric coherence

$$\mathbf{r} = \frac{E\{S_1 S_2^H\}}{\sqrt{\bar{I}_1 \bar{I}_2}} = |\mathbf{r}| e^{j\phi_0}$$

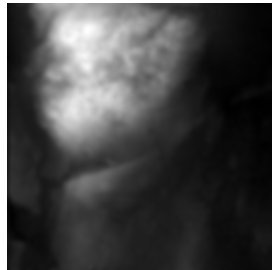
$|\mathbf{r}|$  indicator of the interferometric information quality

$|\mathbf{r}| = 1$  interferometric assumptions are fulfilled

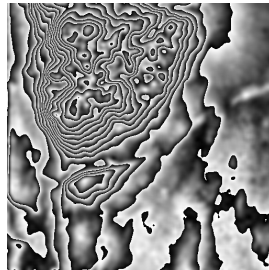
$|\mathbf{r}| = 0$  interferometric images are totally uncorrelated

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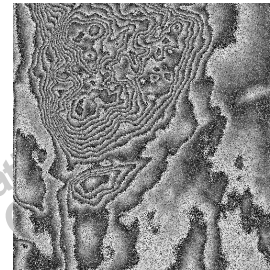
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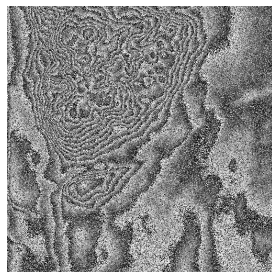
Absolute «True» Phase



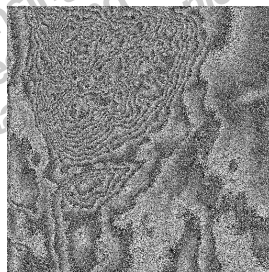
Coherence=1.0



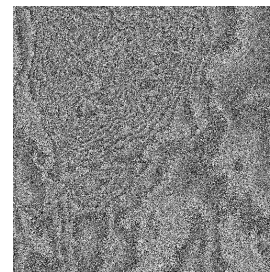
Coherence=0.8



Coherence=0.6



Coherence=0.4



Coherence=0.2

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Polarimetry represents a **cornerstone** for the scatterers analysis

- Polarimetric data allows a **better characterization** of the scatterer being imaged
- Polarimetric data is basically sensitive to the **geometry** and the **electrical properties** of the scatterer being imaged
- **Polarimetric synthesis allows**, from the response of the scatterer to a particular polarization basis, the response to any polarization basis

### SAR Polarimetry

- Extend the advantages of SAR systems, mainly, the high spatial resolution, to polarimetric data
- Considerations
  - Wave polarimetry
  - Wave scattering
  - Target Decomposition Theorems

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Polarimetry is the most clear example of the Electromagnetic Waves' vectorial nature

■ Electric field description

Real electric field vector  $\vec{E}(z,t) = \Re(\underline{E}(z)e^{j\omega t})$  Harmonic time dependence

Complex electric field vector  $\underline{E}(z)$

Helmutz Propagation Equation

$$\nabla^2 \underline{E}(z) + k^2 \underline{E}(z) = 0$$

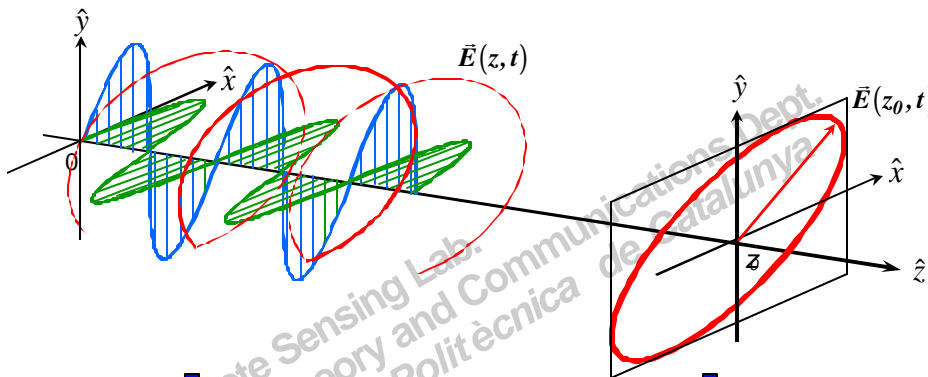
General Solution

$$\underline{E}(z) = \underline{E} e^{-jkz}$$

With:  $\underline{E} = \begin{bmatrix} E_x \\ E_y \\ E_z \end{bmatrix} = \begin{bmatrix} E_{ox} e^{jd_x} \\ E_{oy} e^{jd_y} \\ E_{oz} e^{jd_z} \end{bmatrix}$

Sinusoidal Plane Wave

$$\nabla \cdot \vec{E}(z,t) = 0 \Rightarrow \frac{\partial E_z}{\partial z} = 0$$



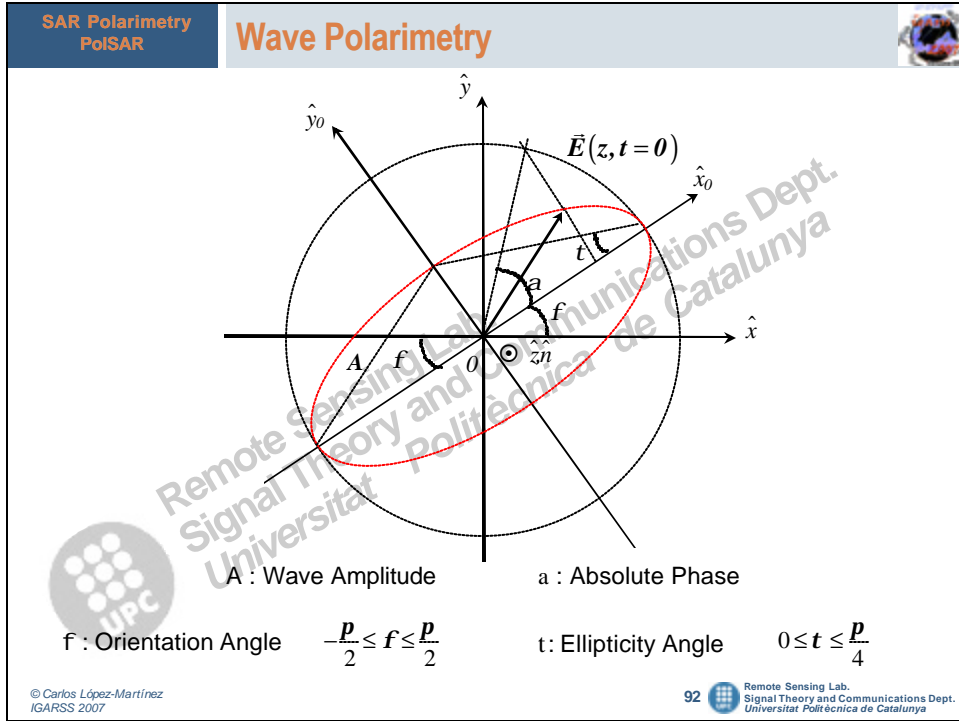
Real electric field vector

$$\vec{E}(z,t) = \begin{cases} E_x = E_{0x} \cos(\omega t - kz - d_x) \\ E_y = E_{0y} \cos(\omega t - kz - d_y) \\ E_z = 0 \end{cases}$$

Polarization ellipse

$$\left(\frac{E_x}{E_{0x}}\right)^2 - 2 \frac{E_x E_y}{E_{0x} E_{0y}} \cos(d) + \left(\frac{E_y}{E_{0y}}\right)^2 = \sin^2(d)$$

With:  $d = d_x - d_y$



**SAR Polarimetry**  
**PoSAR**

## Wave Polarimetry

Representation of the wave polarization state with the **minimum amount** of information

Real electric field vector

$$\vec{E}(z, t) = \begin{cases} E_x = E_{0x} \cos(\omega t - kz - \mathbf{d}_x) \\ E_y = E_{0y} \cos(\omega t - kz - \mathbf{d}_y) \\ E_z = 0 \end{cases}$$

$\vec{E}(z, t) = \Re \left( \underline{E} e^{j(\omega t - kz)} \right)$

Phasor = Jones Vector

$$\underline{E} = \begin{bmatrix} E_x = E_{0x} e^{j\mathbf{d}_x} \\ E_y = E_{0y} e^{j\mathbf{d}_y} \end{bmatrix}$$

Jones vector does not contain neither **time** nor **propagation** information

Polarization ellipse geometrical **parameters**

**Absolute Phase**  $\mathbf{a} = \mathbf{d}_x$

**Wave Amplitude**  $A = \sqrt{E_{0x}^2 + E_{0y}^2}$

**Orientation Angle**  $\tan 2f = 2 \frac{E_{0x} E_{0y}}{E_{0x}^2 - E_{0y}^2} \cos \mathbf{d}$

**Polarization handedness**  $\text{Sign}(t)$

**Ellipticity Angle**  $\sin 2t = 2 \frac{E_{0x} E_{0y}}{E_{0x}^2 + E_{0y}^2} \sin \mathbf{d}$

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**SAR Polarimetry**  
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## Wave Polarimetry

**Deterministic Scattering**  
Completely Polarized Wave

**Random Scattering**  
Partially Polarized Wave

Polarisation Ellipse varies in time/space  
Amplitude, Phase: Random processes

**Statistical description needed**

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**SAR Polarimetry**  
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## Wave Polarimetry

Random electromagnetic fields  $\Rightarrow$

$$E\{E_x\} = 0$$

$$E\{E_y\} = 0$$

Wave polarization descriptors based on first order moments (field) **not valid** to describe partially polarized waves

Jones vector varies in time/space  $\underline{E}(t) = \begin{bmatrix} E_{ox}(t)e^{jd_x(t)} \\ E_{oy}(t)e^{jd_y(t)} \end{bmatrix}$

**Wave polarization descriptors based on higher order moments**

- Stokes Vector
- Wave Covariance Matrix

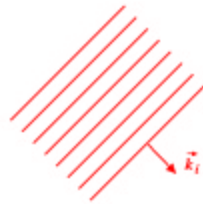
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What is the objective to employ wave polarimetry?

Incident Wave  
 $\vec{E}^i(\vec{r}) = \vec{E}_0^i e^{j(k_r r)}$



Far Field Approximation

$$\vec{E}^s(\vec{r}) = \vec{E}_0^s e^{j(k_r r)}$$

$$|\vec{r}| \gg |\vec{r}'|$$

and

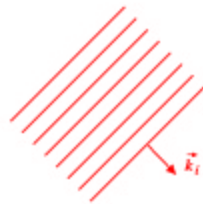
$$|\vec{r}| \gg \lambda$$

The scatterer under study reacts differently to incident waves different polarization states. Hence, the relation between the incident and the scattered waves permits to analyze and characterize the scatterer.



What is the objective to employ wave polarimetry?

Incident Wave  
 $\vec{E}^i(\vec{r}) = \vec{E}_0^i e^{j(k_r r)}$



Far Field Approximation

$$\vec{E}^s(\vec{r}) = \vec{E}_0^s e^{j(k_r r)}$$

$$|\vec{r}| \gg |\vec{r}'|$$

and

$$|\vec{r}| \gg \lambda$$

Scattered Jones Vector

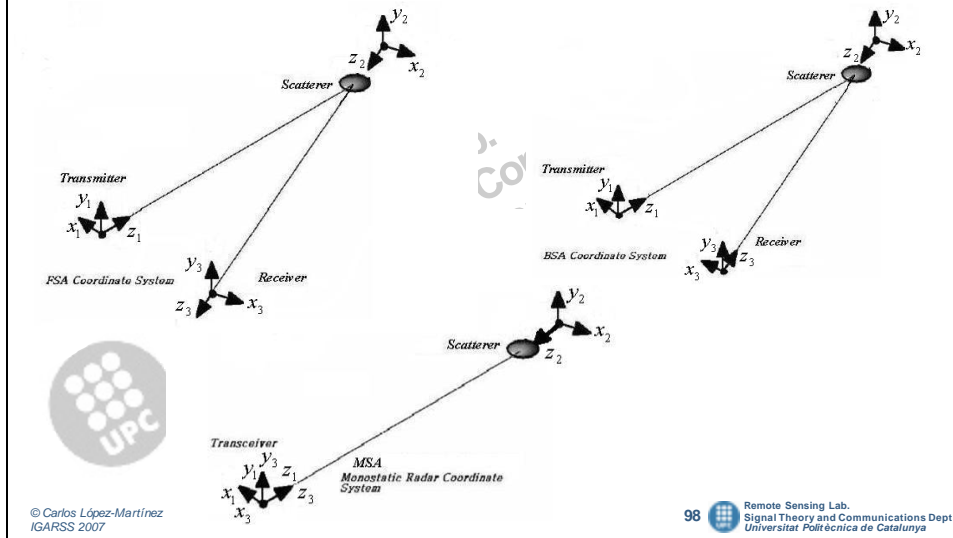
$$\begin{bmatrix} E_{\perp}^s(\vec{r}) \\ E_{\parallel}^s(\vec{r}) \end{bmatrix} = \frac{e^{jkr}}{r} \begin{bmatrix} S_{\perp\perp}(\vec{r}) & S_{\perp\parallel}(\vec{r}) \\ S_{\parallel\perp}(\vec{r}) & S_{\parallel\parallel}(\vec{r}) \end{bmatrix} \begin{bmatrix} E_{\perp}^i(\vec{r}) \\ E_{\parallel}^i(\vec{r}) \end{bmatrix}$$

2x2 Complex Scattering matrix

Incident Jones Vector



It is necessary to establish a **scattering coordinate framework** since the scattering problem deals with (complex vectorial) quantities



**Bistatic Case:** Scattering or Jones matrix

$$\begin{bmatrix} E_X^s \\ E_Y^s \end{bmatrix} = \frac{e^{ikr}}{r} \begin{bmatrix} S_{XX} & S_{XY} \\ S_{YX} & S_{YY} \end{bmatrix} \begin{bmatrix} E_X^i \\ E_Y^i \end{bmatrix}$$

- X and Y are a pair of orthogonal polarization states
- Defined in the local coordinates system
- [S] is **independent** of the polarisation of the incident wave
- [S] is **dependent** on the frequency, the geometrical and electrical properties of the scatterer
- Total scattered power

$$Span(\mathbf{S}) = Trace(\mathbf{S}\mathbf{S}^H) = |S_{XX}|^2 + |S_{XY}|^2 + |S_{YX}|^2 + |S_{YY}|^2$$





$$\mathbf{S} = \frac{e^{jkr}}{r} \begin{bmatrix} S_{XX} & S_{XY} \\ S_{YX} & S_{YY} \end{bmatrix} = \frac{e^{jkr}}{r} \begin{bmatrix} |S_{XX}| e^{j\phi_{XX}} & |S_{XY}| e^{j\phi_{XY}} \\ |S_{YX}| e^{j\phi_{YX}} & |S_{YY}| e^{j\phi_{YY}} \end{bmatrix}$$

↓ Absolute Scattering Matrix

$$\mathbf{S} = \frac{e^{jkr} e^{j\phi_{XX}}}{r} \begin{bmatrix} |S_{XX}| & |S_{XY}| e^{j(\phi_{XY} - \phi_{XX})} \\ |S_{YX}| e^{j(\phi_{YX} - \phi_{XX})} & |S_{YY}| e^{j(\phi_{YY} - \phi_{XX})} \end{bmatrix}$$

Absolute phase factor

Relative Scattering Matrix  
Seven Parameters: 4 amplitudes and 3 phase



**SCATTERER POLARIMETRIC DIMENSION = 7**



Monostatic Case: Backscattering or Sinclair matrix

- In the case of Backscattering from reciprocal scatterers

RECIPROCITY THEOREM  $\mathbf{S}_{XY}^{BSA} = \mathbf{S}_{YX}^{BSA} \quad \hat{\mathbf{U}} \quad \mathbf{S}_{XY}^{FSA} = -\mathbf{S}_{YX}^{FSA}$



$$\begin{bmatrix} E_X^s \\ E_Y^s \end{bmatrix} = \frac{e^{jkr}}{r} \begin{bmatrix} S_{XX} & S_{XY} \\ S_{XY} & S_{YY} \end{bmatrix} \begin{bmatrix} E_X^i \\ E_Y^i \end{bmatrix}$$

(BSA CONVENTION)

- Total scattered power

$$Span(\mathbf{S}) = Trace(\mathbf{S}\mathbf{S}^{T*}) = |S_{XX}|^2 + 2|S_{XY}|^2 + |S_{YY}|^2$$



$$\mathbf{S} = \frac{e^{jkr}}{r} \begin{bmatrix} S_{XX} & S_{XY} \\ S_{XY} & S_{YY} \end{bmatrix} = \frac{e^{jkr}}{r} \begin{bmatrix} |S_{XX}| e^{j\tilde{f}_{XX}} & |S_{XY}| e^{j\tilde{f}_{XY}} \\ |S_{XY}| e^{j\tilde{f}_{XY}} & |S_{YY}| e^{j\tilde{f}_{YY}} \end{bmatrix}$$

↓ Absolute Scattering Matrix

$$\mathbf{S} = \frac{e^{jkr} e^{j\tilde{f}_{XX}}}{r} \begin{bmatrix} |S_{XX}| & |S_{XY}| e^{j(\tilde{f}_{XY} - \tilde{f}_{XX})} \\ |S_{XY}| e^{j(\tilde{f}_{XY} - \tilde{f}_{XX})} & |S_{YY}| e^{j(\tilde{f}_{YY} - \tilde{f}_{XX})} \end{bmatrix}$$

Absolute phase factor

Relative Scattering Matrix  
Seven Parameters: 3 amplitudes and 2 phase



**SCATTERER POLARIMETRIC DIMENSION = 5**



Vectorial formulation of the scattering problem

$$\mathbf{S} = \begin{bmatrix} S_{XX} & S_{XY} \\ S_{YX} & S_{YY} \end{bmatrix}$$



$$\mathbf{k} = V(\mathbf{S}) = \frac{1}{2} \text{Trace}(\mathbf{S} \mathbf{?}) = \begin{bmatrix} S_1 \\ S_2 \\ S_3 \\ S_4 \end{bmatrix} \in \mathbb{C}_4$$

Vectorization process

Scattering vector

With:  $V(\mathbf{S})$  Matrix Vectorization Operator  
? Set of orthogonal 2x2 matrices

Frobenius norm of:  $\mathbf{S}$

$$\begin{aligned} \|\mathbf{S}\|^2 &= \mathbf{S}^H \cdot \mathbf{S} = |S_1|^2 + |S_2|^2 + |S_3|^2 + |S_4|^2 \\ &= \text{Span}(\mathbf{S}) = |S_{XX}|^2 + |S_{YX}|^2 + |S_{XY}|^2 + |S_{YY}|^2 \end{aligned}$$



Pauli scattering vector  $\mathbf{k}_p = V(\mathbf{S}) = \frac{1}{2} \text{Trace}(\mathbf{S} \cdot \mathbf{?}_p)$

Set of 2x2 complex matrices from the Pauli matrices group

$$\mathbf{?}_p = \left\{ \sqrt{2} \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}, \sqrt{2} \begin{bmatrix} 1 & 0 \\ 0 & -1 \end{bmatrix}, \sqrt{2} \begin{bmatrix} 0 & 1 \\ 1 & 0 \end{bmatrix}, \sqrt{2} \begin{bmatrix} 0 & -j \\ j & 0 \end{bmatrix} \right\}$$



Bistatic case  $\mathbf{k}_p = \frac{1}{\sqrt{2}} \begin{bmatrix} S_{XX} + S_{YY} \\ S_{XX} - S_{YY} \\ S_{XY} + S_{YX} \\ j(S_{XY} - S_{YX}) \end{bmatrix}$

Monostatic case  $\mathbf{k}_p = \frac{1}{\sqrt{2}} \begin{bmatrix} S_{XX} + S_{YY} \\ S_{XX} - S_{YY} \\ 2S_{XY} \end{bmatrix}$

Advantage: Closer related to physical properties of the scatterer

Note: Also known as  $\mathbf{k}_{4P}$  or  $\mathbf{k}_{3P}$



Lexicographic scattering vector  $\mathbf{k} = V(\mathbf{S}) = \frac{1}{2} \text{Trace}(\mathbf{S} \cdot \mathbf{?}_L)$

Set of 2x2 complex matrices from the Lexicographic matrices group

$$\mathbf{?}_L = \left\{ 2 \begin{bmatrix} 1 & 0 \\ 0 & 0 \end{bmatrix}, 2 \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix}, 2 \begin{bmatrix} 0 & 0 \\ 1 & 0 \end{bmatrix}, 2 \begin{bmatrix} 0 & 0 \\ 0 & 1 \end{bmatrix} \right\}$$



Bistatic case  $\mathbf{k} = \begin{bmatrix} S_{XX} \\ S_{XY} \\ S_{YX} \\ S_{YY} \end{bmatrix}$

Monostatic case  $\mathbf{k} = \begin{bmatrix} S_{XX} \\ \sqrt{2}S_{XY} \\ S_{YY} \end{bmatrix}$

Advantage: Directly related to the system measurables

Note: Also known as  $\mathbf{k}_{4L}$  or  $\mathbf{k}_{3L}$



Bistatic Pauli scattering vector  $\mathbf{k}_p = \frac{1}{\sqrt{2}} [S_{XX} + S_{YY} \quad S_{XX} - S_{YY} \quad S_{XY} + S_{YX} \quad j(S_{XY} - S_{YX})]^T$

Coherency matrix  $\Rightarrow \mathbf{T} = \mathbf{k}_p \mathbf{k}_p^* = \begin{bmatrix} 2A_0 & C - jD & H + jG & L - jK \\ C + jD & B_0 + B & E + jF & M - jN \\ H - jG & E - jF & B_0 - B & J + jI \\ L + jK & M + jN & J - jI & 2A \end{bmatrix}$

Monostatic Pauli scattering vector  $\mathbf{k} = \frac{1}{\sqrt{2}} [S_{XX} + S_{YY} \quad S_{XX} - S_{YY} \quad 2S_{XY}]^T$

Coherency matrix  $\Rightarrow \mathbf{T} = \mathbf{k}_p \mathbf{k}_p^* = \begin{bmatrix} 2A_0 & C - jD & H + jG \\ C + jD & B_0 + B & E + jF \\ H - jG & E - jF & B_0 - B \end{bmatrix}$

**Hermitian positive semi definite matrix – Rank 1**



Bistatic Lexicographic scattering vector  $\mathbf{k} = [S_{XX} \quad S_{XY} \quad S_{YX} \quad S_{YY}]^T$

Covariance matrix  $\Rightarrow \mathbf{C} = \mathbf{k} \mathbf{k}^H = \begin{bmatrix} S_{XX} S_{XX}^* & S_{XX} S_{XY}^* & S_{XX} S_{YX}^* & S_{XX} S_{YY}^* \\ S_{XY} S_{XX}^* & S_{XY} S_{XY}^* & S_{XY} S_{YX}^* & S_{XY} S_{YY}^* \\ S_{YX} S_{XX}^* & S_{YX} S_{XY}^* & S_{YX} S_{YX}^* & S_{YX} S_{YY}^* \\ S_{YY} S_{XX}^* & S_{YY} S_{XY}^* & S_{YY} S_{YX}^* & S_{YY} S_{YY}^* \end{bmatrix}$

Monostatic Lexicographic scattering vector  $\mathbf{k} = [S_{XX} \quad \sqrt{2}S_{XY} \quad S_{YY}]^T$

Covariance matrix  $\Rightarrow \mathbf{C} = \mathbf{k} \mathbf{k}^H = \begin{bmatrix} S_{XX} S_{XX}^* & \sqrt{2}S_{XX} S_{XY}^* & S_{XX} S_{YY}^* \\ \sqrt{2}S_{XY} S_{XX}^* & 2S_{XY} S_{XY}^* & \sqrt{2}S_{XY} S_{YY}^* \\ S_{YY} S_{XX}^* & \sqrt{2}S_{YY} S_{XY}^* & S_{YY} S_{YY}^* \end{bmatrix}$

**Hermitian positive semi definite matrix – Rank 1**

**SAR Polarimetry**  
PoISAR

## Polarimetric Wave Scattering

**Deterministic Scattering**  
Completely Polarized Scattering

**Random Scattering**  
Partially Polarized Scattering

Can not be described by  $S, k_p, k$

**Necessity of statistical descriptors**

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**SAR Polarimetry**  
PoISAR

## Polarimetric Wave Scattering

Relations for **deterministic** scattering

**S**  
SINCLAIR  
 $SU(2)$

**C**      **T**  
COVARIANCE COHERENCY  
 $SU(3)$        $SU(3)$

**K**  
KENNAUGH  
 $O(4)$

All polarimetric descriptors contain the same information !!!

All polarimetric descriptors the same number of independent parameters !!!  
(Bistatic 7 – Monostatic 5)

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Relations for **random** scattering

Data **must** be averaged

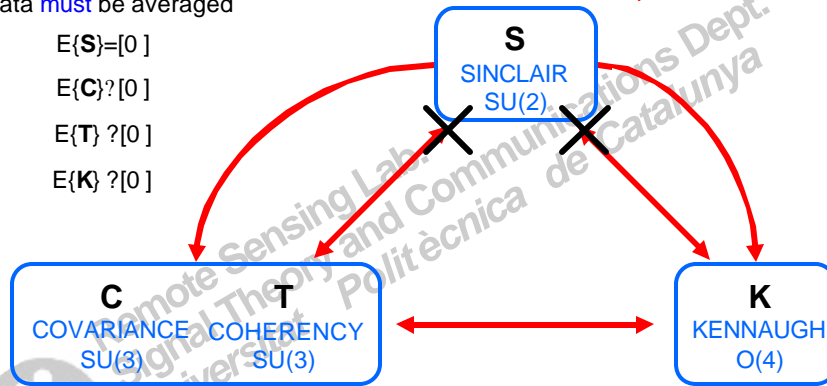
$$E\{\mathbf{S}\} = [0]$$

$$E\{\mathbf{C}\} \neq [0]$$

$$E\{\mathbf{T}\} \neq [0]$$

$$E\{\mathbf{K}\} \neq [0]$$

Independent parameters !!!  
(Bistatic 7 – Monostatic 5)  
Absolute phase is not considered



Independent parameters !!!  
(Bistatic 16 – Monostatic 9)

[S] is not a statistical descriptor, it is a zero-mean multidimensional random value !!!



PolSARpro v3.0 Software:

Tool specifically designed to handle **Polarimetric** data.

**Educational Software** offering a tool for **self-education** in the field of Polarimetric SAR and Interferometric Polarimetric SAR data processing and analysis.

Developed to be accessible to a wide range of users, from **novices** to **experts** in the field of Polarimetry.

## Software: PolSARPro v3.0



Visit regularly the Web Site  
<http://earth.esa.int/polsarpro>

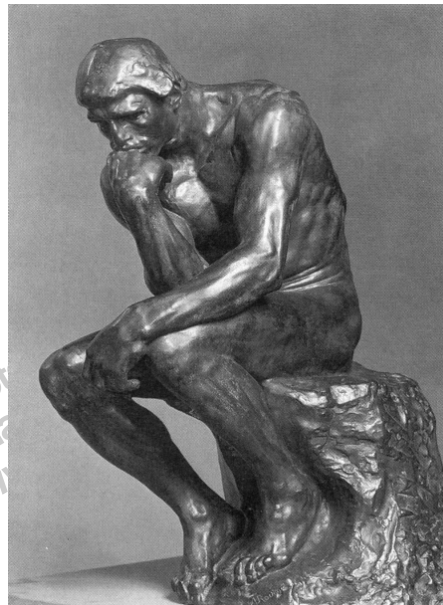
The Web Site provides

- Details of the project
- Access to the tutorial and software
- Information about status of the development
- Demonstration Sample Datasets
- Recently obtained results

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**Polarimetric SAR Interferometry**

Polarimetry and Interferometry are **complementary information**

$|HH+VV|$     $|HH-VV|$     $|HV|$

$|g_w|$

DLR E-SAR L Band  
POL-InSAR (1.5m x 3m)  
Baseline 5m

- Polarimetry provides sensitivity to **scattering mechanisms**
- Interferometry provides sensitivity to **height information**

**Location of scattering mechanism in height**

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PolInSAR data mathematical representation

- (6x6) coherency matrix  $\langle \mathbf{T}_6 \rangle$

$$\mathbf{k} = \begin{bmatrix} \mathbf{k}_1 \\ \mathbf{k}_2 \end{bmatrix} \Rightarrow \langle \mathbf{T}_6 \rangle = \langle \mathbf{k} \mathbf{k}^\dagger \rangle = \begin{bmatrix} \langle \mathbf{T}_1 \rangle & \langle \mathbf{O}_{12} \rangle \\ \langle \mathbf{O}_{12} \rangle^\dagger & \langle \mathbf{T}_2 \rangle \end{bmatrix}$$

$\langle \mathbf{T}_1 \rangle$  and  $\langle \mathbf{T}_2 \rangle$  separate image coherency matrices

$\langle \mathbf{O}_{12} \rangle$  correlation matrix

- Coherence set in the radar polarization basis

$$(\mathbf{r}_1, \mathbf{r}_2, \mathbf{r}_3) \text{ with } \mathbf{r}_i = \frac{\langle k_{1i} \ k_{2i}^* \rangle}{\sqrt{\langle k_{1i} \ k_{1i}^* \rangle \langle k_{2i} \ k_{2i}^* \rangle}} \text{ for } i = 1, 2, 3$$



PolInSAR data mathematical representation

- Coherence representation using projection vectors

$$k_{1i} = \mathbf{w}_i^{*T} \mathbf{k}_1, \quad k_{2i} = \mathbf{w}_i^{*T} \mathbf{k}_2, \quad r_i = \frac{\langle k_{1i} \ k_{2i}^* \rangle}{\sqrt{\langle k_{1i} \ k_{1i}^* \rangle \langle k_{2i} \ k_{2i}^* \rangle}}$$

$$r_i = \frac{\langle \mathbf{w}_i^{*T} \mathbf{k}_1 \ \mathbf{k}_2^{*T} \mathbf{w}_i \rangle}{\sqrt{\langle \mathbf{w}_i^{*T} \mathbf{k}_1 \ \mathbf{k}_1^{*T} \mathbf{w}_i \rangle \langle \mathbf{w}_i^{*T} \mathbf{k}_2 \ \mathbf{k}_2^{*T} \mathbf{w}_i \rangle}} = \frac{\mathbf{w}_i^{*T} \langle \mathbf{O}_{12} \rangle \mathbf{w}_i}{\sqrt{\mathbf{w}_i^{*T} \langle \mathbf{T}_{11} \rangle \mathbf{w}_i \ \mathbf{w}_i^{*T} \langle \mathbf{T}_{22} \rangle \mathbf{w}_i}}$$

- Coherence set in an arbitrary polarization basis

$$\mathbf{k}'_1 = \mathbf{U}_{\text{SU3}} \mathbf{k}_1, \quad \mathbf{k}'_2 = \mathbf{U}_{\text{SU3}} \mathbf{k}_2, \quad r(\mathbf{w}) = \frac{\mathbf{w}^{*T} \langle \mathbf{O}_{12} \rangle \mathbf{w}}{\sqrt{\mathbf{w}^{*T} \langle \mathbf{T}_{11} \rangle \mathbf{w} \ \mathbf{w}^{*T} \langle \mathbf{T}_{22} \rangle \mathbf{w}}}$$

- Coherence set in different emission/reception polarization basis

$$r(\mathbf{w}_p, \mathbf{w}_2) = \frac{\mathbf{w}_1^{*T} \langle \mathbf{O}_{12} \rangle \mathbf{w}_2}{\sqrt{\mathbf{w}_1^{*T} \langle \mathbf{T}_{11} \rangle \mathbf{w}_1 \ \mathbf{w}_2^{*T} \langle \mathbf{T}_{22} \rangle \mathbf{w}_2}}$$





Optimal coherence set

$$\text{Interferometric coherence } r(\mathbf{w}_1, \mathbf{w}_2) = \frac{\mathbf{w}_1^{*T} \langle \mathbf{O}_{12} \rangle \mathbf{w}_2}{\sqrt{\mathbf{w}_1^{*T} \langle \mathbf{T}_{11} \rangle \mathbf{w}_1 \mathbf{w}_2^{*T} \langle \mathbf{T}_{22} \rangle \mathbf{w}_2}}$$

Which polarization combination leads to the maximum possible interferometric coherence?

$$L = \mathbf{w}_1^{*T} \langle \mathbf{O}_{12} \rangle \mathbf{w}_2 + I_1 (\mathbf{w}_1^{*T} \langle \mathbf{T}_{11} \rangle \mathbf{w}_1 - C_1) + I_2 (\mathbf{w}_2^{*T} \langle \mathbf{T}_{22} \rangle \mathbf{w}_2 - C_2)$$

$$\max_{\mathbf{w}_1, \mathbf{w}_2} (LL^*)$$

$$\frac{\partial L}{\partial \mathbf{w}_1^{*T}} = \langle \mathbf{O}_{12} \rangle \mathbf{w}_2 + I_1 \langle \mathbf{T}_{11} \rangle \mathbf{w}_1 = 0 \quad \Rightarrow \quad \langle \mathbf{T}_{11} \rangle^{-1} \langle \mathbf{O}_{12} \rangle \langle \mathbf{T}_{22} \rangle^{-1} \langle \mathbf{O}_{12} \rangle^{*T} \mathbf{w}_1 = \mathbf{n} \mathbf{w}_1$$

$$\frac{\partial L}{\partial \mathbf{w}_2^{*T}} = \langle \mathbf{O}_{12} \rangle^{*T} \mathbf{w}_1 + I_2 \langle \mathbf{T}_{22} \rangle \mathbf{w}_2 = 0 \quad \Rightarrow \quad \langle \mathbf{T}_{22} \rangle^{-1} \langle \mathbf{O}_{12} \rangle^{*T} \langle \mathbf{T}_{11} \rangle^{-1} \langle \mathbf{O}_{12} \rangle \mathbf{w}_2 = \mathbf{n} \mathbf{w}_2$$

These matrices are not hermitian, but  $\mathbf{n} = I_1 I_2^*$  is real



Optimal coherence set

$$\text{Coherence optimisation } \begin{aligned} \langle \mathbf{T}_{11} \rangle^{-1} \langle \mathbf{O}_{12} \rangle \langle \mathbf{T}_{22} \rangle^{-1} \langle \mathbf{O}_{12} \rangle^{*T} \mathbf{w}_1 &= \mathbf{n} \mathbf{w}_1 \\ \langle \mathbf{T}_{22} \rangle^{-1} \langle \mathbf{O}_{12} \rangle^{*T} \langle \mathbf{T}_{11} \rangle^{-1} \langle \mathbf{O}_{12} \rangle \mathbf{w}_2 &= \mathbf{n} \mathbf{w}_2 \end{aligned}$$



Three real eigenvalues

$$\mathbf{n}_1 \geq \mathbf{n}_2 \geq \mathbf{n}_3$$

Three pairs of eigenvectors

$$(\mathbf{w}_{11}, \mathbf{w}_{12}), (\mathbf{w}_{21}, \mathbf{w}_{22}), (\mathbf{w}_{31}, \mathbf{w}_{32})$$

- Optimum coherence values  $r_i = \sqrt{\mathbf{n}_i}$
- Optimum scattering mechanisms  $(\mathbf{w}_{i1}, \mathbf{w}_{i2})$

Image formation

$$\mathbf{m}_1 = \mathbf{w}_{11}^{*T} \mathbf{k}_1 \quad \mathbf{m}_2 = \mathbf{w}_{21}^{*T} \mathbf{k}_2$$

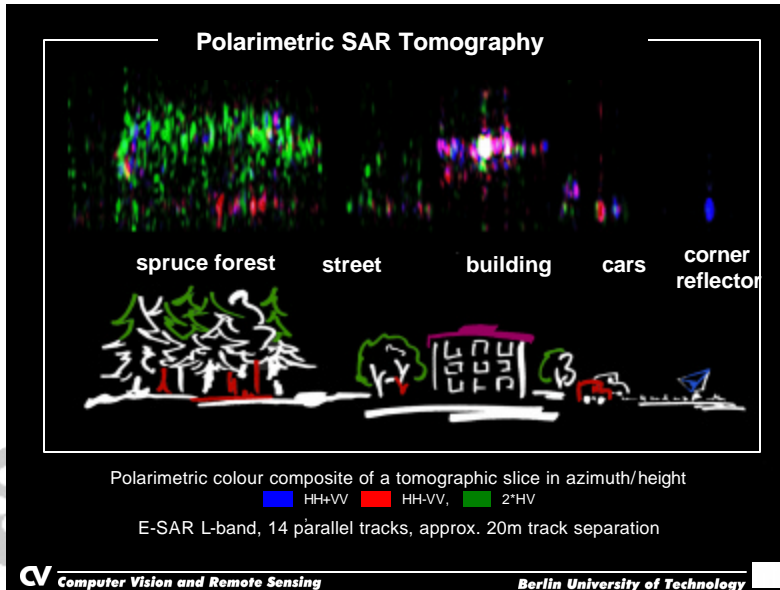
Eigen phase normalisation

$$\mathbf{f}_e = \arg(\mathbf{w}_{11}^{*T} \mathbf{w}_{21}) = 0$$

Interferogram

$$\mathbf{m}_1 \mathbf{m}_2^* = (\mathbf{w}_{11}^{*T} \mathbf{k}_1) (\mathbf{w}_{21}^{*T} \mathbf{k}_2)^* = \mathbf{w}_{11}^{*T} \langle \mathbf{O}_{12} \rangle \mathbf{w}_{21}$$

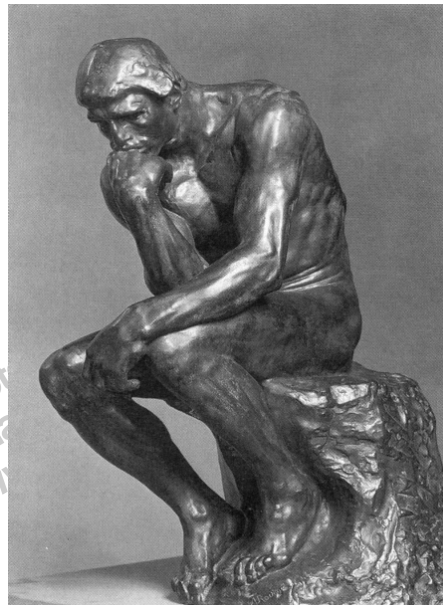
# Polarimetric SAR Tomography



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**Multidimensional SAR Data Models**

Multidimensional SAR systems present a wide spectra of configurations

- SAR Interferometry
- Differential SAR interferometry
- SAR Polarimetry
- Polarimetric SAR Interferometry
- SAR Tomography/ Multibaseline
- Multitemporal SAR
- Multifrequency SAR

How to deal with all these types of configurations?

- **Statistics:** Speckle noise imposes the use of statistical descriptors
  - Speckle affects the SAR images
  - Speckle affects the correlation structure
- **Physics:** The interpretation of the data must be done according to the physics behind the imaging process

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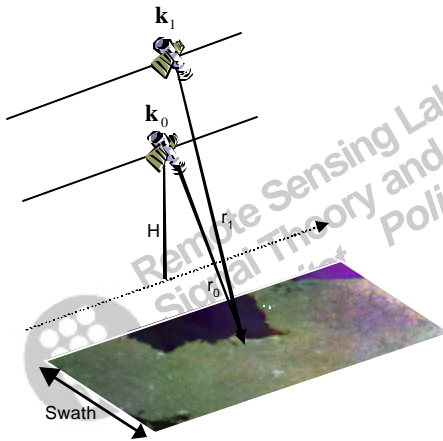
**Electromagnetic Signal Processing**

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The multidimensional SAR system acquires  $m$  complex SAR images

Target vector  $\mathbf{k} = [S_1, S_2, \dots, S_m]^T$



The properties of the target vector follow from the properties of a single SAR image

- $\mathbf{k}$  is **deterministic** for **point scatterers**. It contains all the necessary information to characterize the scatterer
- $\mathbf{k}$  is a **multidimensional random variable** for **distributed scatterers** due to **speckle**. A single sample does not characterize the scatterer

SAR images characterized through second order moments

- **Second order moments** in multidimensional SAR data are **matrix quantities**



PDF for **non-correlated** SAR images (Distributed scatterers)

- Zero-mean multidimensional complex (also circular) Gaussian pdf

$$p_{\mathbf{k}}(\mathbf{k}) = \prod_{k=1}^m \frac{1}{p\mathbf{s}^2} \exp\left(-\frac{S_k S_k^H}{\mathbf{s}^2}\right) = \frac{1}{p^m \mathbf{s}^{2m}} \exp\left(-\sum_{k=1}^m \frac{S_k S_k^H}{\mathbf{s}^2}\right) = \frac{1}{p^m \mathbf{s}^{2m}} \exp\left(-\frac{1}{\mathbf{s}^2} \text{tr}(\mathbf{k}\mathbf{k}^H)\right)$$

↑  
Independent SAR images with the same power  $S_k = \mathcal{N}_{C^2}(0, \mathbf{s}^2/2)$

- First order moment

$$E\{\mathbf{k}\} = \mathbf{0}$$

- Second order moment: Covariance matrix

$$\mathbf{C} = E\{\mathbf{k}\mathbf{k}^H\} = \mathbf{s}^{-2} \mathbf{I}_{m \times m}$$



Characterization of random variables

- Probability Density Function (pdf)
- Moment-generating function
- Statistical moments (mean, power, kurtosis, skewness...)

Zero-mean multidimensional complex Gaussian pdf

$$p_{\mathbf{k}}(\mathbf{k}) = \frac{1}{\pi^m |\mathbf{C}|} \exp(-\mathbf{k}^H \mathbf{C}^{-1} \mathbf{k})$$

- First order moment  $E\{\mathbf{k}\} = \mathbf{0}$
- Second order moment: Covariance matrix

$$\mathbf{C} = E\{\mathbf{k}\mathbf{k}^H\} = \begin{bmatrix} E\{S_1 S_1^H\} & E\{S_1 S_2^H\} & \cdots & E\{S_1 S_m^H\} \\ E\{S_2 S_1^H\} & E\{S_2 S_2^H\} & \cdots & E\{S_2 S_m^H\} \\ \vdots & \vdots & \ddots & \vdots \\ E\{S_m S_1^H\} & E\{S_m S_2^H\} & \cdots & E\{S_m S_m^H\} \end{bmatrix} \quad E\{S_k S_l^*\} \neq 0 \quad k, l \in \{1, \dots, m\}, k \neq l$$



Correlated SAR images



A zero-mean multidimensional complex Gaussian pdf is completely characterized by the second order moments, i.e., the covariance matrix

- **Moment theorem** for complex Gaussian processes, given  $Q$  correlated SAR images

- For  $k \neq l$ , where  $m_k$  and  $n_l$  are integers from  $\{1, 2, \dots, Q\}$

$$E\{S_{m_1} S_{m_2} \cdots S_{m_k} S_{n_1}^* S_{n_2}^* \cdots S_{n_l}^*\} = 0$$

- For  $k = l$ , where  $p$  is a permutation of the set of integers  $\{1, 2, \dots, Q\}$

$$E\{S_{m_1} S_{m_2} \cdots S_{m_k} S_{n_1}^* S_{n_2}^* \cdots S_{n_l}^*\} = \sum_p E\{S_{m_{p(1)}} S_{n_1}^*\} E\{S_{m_{p(2)}} S_{n_2}^*\} \cdots E\{S_{m_{p(l)}} S_{n_l}^*\}$$

- Considering the **covariance matrix**
  - Higher order moments are function of the covariance matrix



The covariance matrix contains the **correlation structure** of the set of  $m$  SAR images

$$\mathbf{C} = E\{\mathbf{k}\mathbf{k}^H\} = \begin{bmatrix} E\{S_1 S_1^H\} & E\{S_1 S_2^H\} & \cdots & E\{S_1 S_m^H\} \\ E\{S_2 S_1^H\} & E\{S_2 S_2^H\} & \cdots & E\{S_2 S_m^H\} \\ \vdots & \vdots & \ddots & \vdots \\ E\{S_m S_1^H\} & E\{S_m S_2^H\} & \cdots & E\{S_m S_m^H\} \end{bmatrix}$$

Information

- Diagonal elements: **Power information**

$$E\{S_k S_k^H\} = E\{|S_k|^2\} \quad k \in \{1, 2, \dots, m\}$$

- Off diagonal elements: **Correlation information**

$$E\{S_k S_l^H\} \quad k, l \in \{1, 2, \dots, m\}, k \neq l$$



PDF for **correlated** SAR images (Distributed scatterers)

- Zero-mean multidimensional complex Gaussian pdf

$$p_{\mathbf{k}}(\mathbf{k}) = \frac{1}{\mathbf{p}^m |\mathbf{C}|} \exp(-\mathbf{k}^H \mathbf{C}^{-1} \mathbf{k})$$

- First order moment

$$E\{\mathbf{k}\} = \mathbf{0}$$

- Second order moment: **Covariance matrix**

$$\mathbf{C} = E\{\mathbf{k}\mathbf{k}^H\} = \begin{bmatrix} E\{S_1 S_1^H\} & E\{S_1 S_2^H\} & \cdots & E\{S_1 S_m^H\} \\ E\{S_2 S_1^H\} & E\{S_2 S_2^H\} & \cdots & E\{S_2 S_m^H\} \\ \vdots & \vdots & \ddots & \vdots \\ E\{S_m S_1^H\} & E\{S_m S_2^H\} & \cdots & E\{S_m S_m^H\} \end{bmatrix}$$

All the information characterizing the set of  $m$  SAR Images is contained in the covariance matrix



How to consider the correlation information

- Off-diagonal covariance matrix elements

$$E\{S_k S_l^H\} \quad k, l \in \{1, 2, \dots, m\}, k \neq l$$

- Absolute correlation information

- Complex correlation coefficient

$$r_{k,l} = \frac{E\{S_k S_l^H\}}{\sqrt{E\{|S_k|^2\} \cdot E\{|S_l|^2\}}} = |r_{k,l}| e^{iq_{k,l}} \quad 0 \leq |r_{k,l}| \leq 1 \quad \text{Coherence}$$

$$-p \leq q_{k,l} \leq p$$

- Normalized correlation information

- The complex correlation information represents the most important observable for multidimensional SAR data. Its physical interpretation depends on the multidimensional SAR system configuration



- SAR Interferometry

- Phase  $q_{k,l}$  contains topographic information
- Coherence  $|r_{k,l}|$  is sensitive to different properties of the imaged area
  - Study and retrieval of stem volume over forested areas
  - Study of dry and wet snow covered areas
  - Characterization of glaciers, valleys, and fjord ice

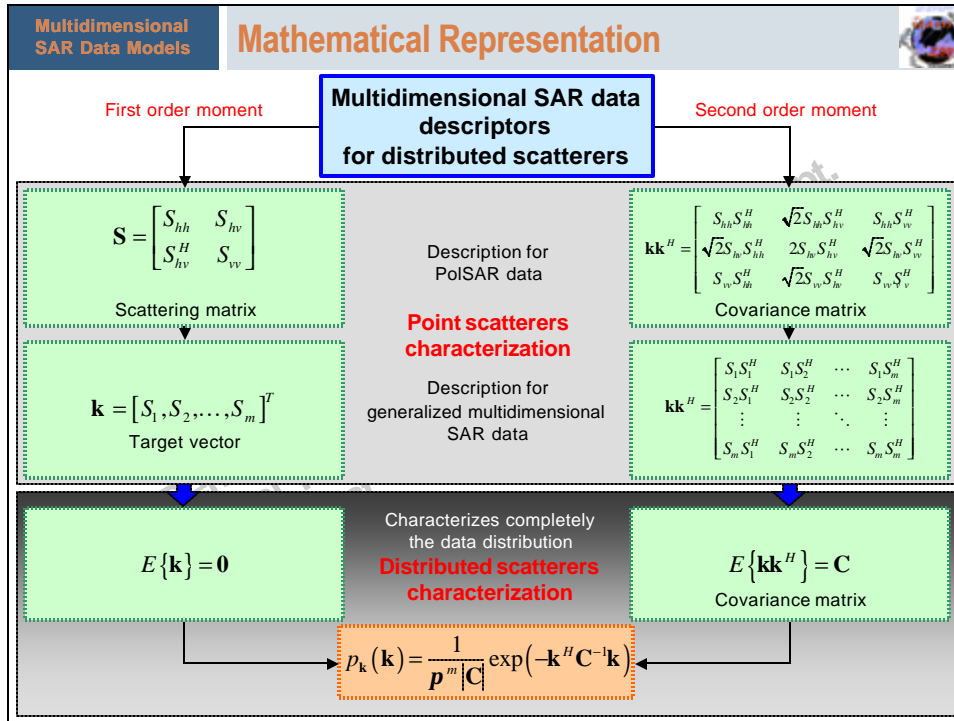
- SAR Polarimetry

- Off-diagonal information related with the geometry and the electrical properties of the target being imaged

- Polarimetric SAR Interferometry

- Complex correlation coefficient related with the vegetation height and the vegetation structural properties





**Multidimensional SAR Data Models**      **Information Estimation/Filtering**

For multidimensional SAR data, under the hypothesis of Gaussian scattering, all the **information** is contained in the **covariance matrix**

$$\mathbf{C} = E\{\mathbf{k}\mathbf{k}^H\} = \begin{bmatrix} E\{S_1S_1^H\} & E\{S_1S_2^H\} & \dots & E\{S_1S_m^H\} \\ E\{S_2S_1^H\} & E\{S_2S_2^H\} & \dots & E\{S_2S_m^H\} \\ \vdots & \vdots & \ddots & \vdots \\ E\{S_mS_1^H\} & E\{S_mS_2^H\} & \dots & E\{S_mS_m^H\} \end{bmatrix}$$

This matrix must be **estimated from the available information**

- The **scattering vector for each pixel/sample** of the SAR data
$$\mathbf{k}_i = [S_1, S_2, \dots, S_m]^T$$
- The estimation process reduces to **estimate the ensemble average (expectation operator)  $E\{\}$**
- The **estimation process** also receives the name of **data filtering process**. In case of homogeneous areas.

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Considerations about speckle noise reduction



Optical image DLR OP



SAR images reflex the Nature's complexity



SAR image DLR OP

Homogeneous areas

Image details

Heterogeneous areas



Maintain useful information (s)

RADIOMETRIC RESOLUTION



Maintain spatial details (Shape and value)

SPATIAL RESOLUTION



Maintain both

LOCAL ANALYSIS



Multidimensional SAR data information estimation, i.e., data filtering, based on two main hypotheses

- **Ergodicity in mean:** The different time/space averages of each process converge to the same limit, i.e., the ensemble average  $E\{\}$ 
  - The statistics in the realizations domain can be calculated in the time/spatial domain
  - Necessary to assume ergodicity since there are not multiple data realizations over the same area
  - Applied to the processes  $E\{|S_k|^2\}$ ,  $E\{|S_l|^2\}$  and  $E\{S_k S_l^H\}$   $k, l \in \{1, 2, \dots, m\}$
- **Wide-sense stationary:** Given a spatial domain all the samples in this spatial domain belong to the same statistical distribution
  - SAR images can not be considered as wide-sense stationary processes since they are a reflex of the data heterogeneity
  - SAR images can be considered **locally wide-sense stationary**
  - Applied to the processes  $E\{|S_k|^2\}$ ,  $E\{|S_l|^2\}$  and  $E\{S_k S_l^H\}$   $k, l \in \{1, 2, \dots, m\}$
- **Homogeneity:** Refers to non-textured data
  - Gaussian distributed data



Covariance matrix estimation by means of a **MultiLook** (BoxCar)

- Maximum likelihood estimator: Sample covariance matrix

$$\mathbf{Z}_n = \frac{1}{n} \sum_{k=1}^n \mathbf{k} \mathbf{k}^H = \begin{bmatrix} \frac{1}{n} \sum_{k=1}^n S_1(k) S_1^*(k) & \frac{1}{n} \sum_{k=1}^n S_1(k) S_2^*(k) & \cdots & \frac{1}{n} \sum_{k=1}^n S_1(k) S_m^*(k) \\ \frac{1}{n} \sum_{k=1}^n S_2(k) S_1^*(k) & \frac{1}{n} \sum_{k=1}^n S_2(k) S_2^*(k) & \cdots & \frac{1}{n} \sum_{k=1}^n S_2(k) S_m^*(k) \\ \vdots & \vdots & \ddots & \vdots \\ \frac{1}{n} \sum_{k=1}^n S_m(k) S_1^*(k) & \frac{1}{n} \sum_{k=1}^n S_m(k) S_2^*(k) & \cdots & \frac{1}{n} \sum_{k=1}^n S_m(k) S_m^*(k) \end{bmatrix}$$

- $n$  represents the total number of samples employed to estimate the covariance matrix, taken a region (square, rectangular, adapted...)
- $\mathbf{Z}_n$  as estimator of  $\mathbf{C}$ 
  - Does not consider signal morphology/heterogeneity
  - Loss of spatial resolution

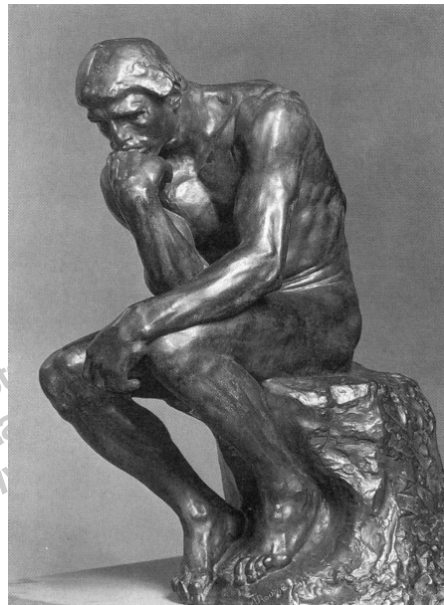
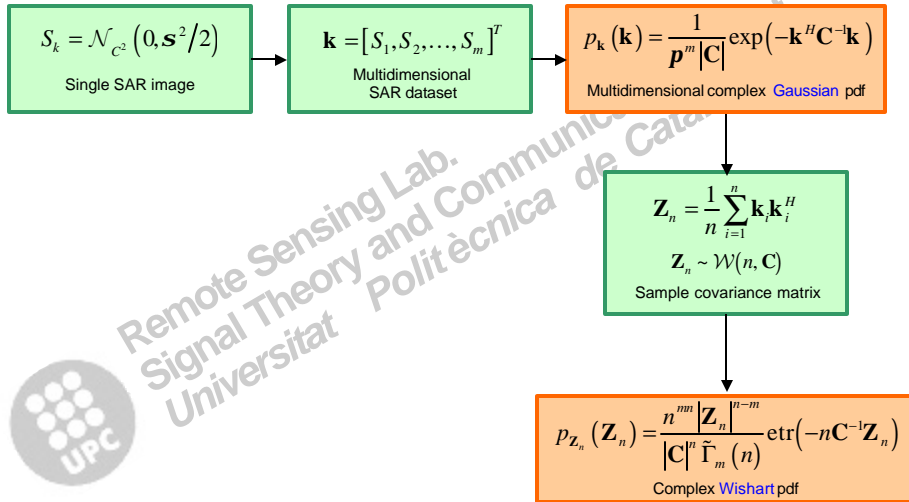
**The sample covariance matrix  $\mathbf{Z}_n$  is itself a multidimensional random variable**



The sample covariance matrix  $\mathbf{Z}_n$  is characterized by the **complex Wishart distribution**  $\mathbf{Z}_n \sim \mathcal{W}(n, \mathbf{C})$

$$p_{\mathbf{Z}_n}(\mathbf{Z}_n) = \frac{n^{nm} |\mathbf{Z}_n|^{n-m}}{|\mathbf{C}|^n \tilde{\Gamma}_m(n)} \text{etr}(-n\mathbf{C}^{-1}\mathbf{Z}_n) \quad \tilde{\Gamma}_m(n) = \mathbf{p}^{m(m-1)/2} \prod_{i=1}^m \Gamma(n-i+1)$$

- Multidimensional data distribution
- Valid for  $n \geq m$ , otherwise  $|\mathbf{Z}_n|^{n-m}$  is equal to zero and the Wishart pdf is undetermined
  - Equivalent to  $\text{Rank}(\mathbf{Z}_n) = m$ , i.e., the sample covariance matrix is a full rank matrix
  - The higher the data dimensionality  $m$  the higher the number of looks  $n$  for the Wishart pdf to be defined





Multidimensional SAR Speckle Models

## Multidimensional Speckle Noise Model

$$\mathbf{kk}^H = \begin{bmatrix} S_1 S_1^H & S_1 S_2^H & \dots & S_1 S_m^H \\ S_2 S_1^H & S_2 S_2^H & \dots & S_2 S_m^H \\ \vdots & \vdots & \ddots & \vdots \\ S_m S_1^H & S_m S_2^H & \dots & S_m S_m^H \end{bmatrix} = \begin{bmatrix} I_1 & S_1 S_2^H & \dots & S_1 S_m^H \\ S_2 S_1^H & I_2 & \dots & S_2 S_m^H \\ \vdots & \vdots & \ddots & \vdots \\ S_m S_1^H & S_m S_2^H & \dots & I_m \end{bmatrix}$$

- Covariance matrix **diagonal elements**
  - Consist of the intensity of the SAR images
  - Speckle noise modelling/reduction as for one dimensional SAR images
$$I_k(x, r) = s_k(x, r) n_k(x, r) \quad k \in \{1, 2, \dots, m\}$$
- Covariance matrix **off-diagonal elements**
  - Consist of the Hermitian products between pairs of SAR images
$$r_{k,l} = \frac{E\{S_k S_l^*\}}{\sqrt{E\{|S_k|^2\} \cdot E\{|S_l|^2\}}} = |r_{k,l}| e^{jq_{k,l}} \quad k, l \in \{1, 2, \dots, m\}$$

A multiplicative speckle noise model can be also considered?

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## Multiplicative speckle noise model extension

- Model for a complex SAR image. Complex image model obtained from the intensity speckle model

$$S_k(x, r) = \sqrt{s_k(x, r)} e^{j\phi_k(x, r)} n_k(x, r) \quad k \in \{1, 2, \dots, m\}$$

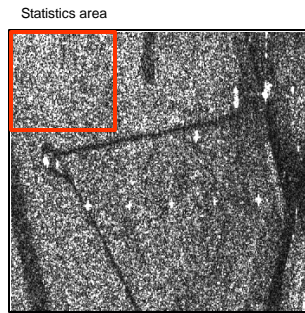
Construction of the covariance matrix terms

$$E\{S_k(x, r) S_l^H(x, r)\} = E\{\sqrt{s_k(x, r) s_l(x, r)} e^{j(\phi_k(x, r) - \phi_l(x, r))}\} E\{n_k(x, r) n_l^H(x, r)\} \quad k, l \in \{1, 2, \dots, m\}$$

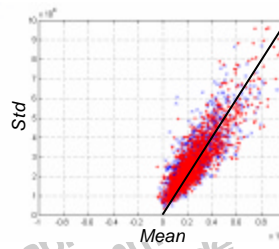
$$I_k = s_k n_k \quad k \in \{1, 2, \dots, m\} \quad \Rightarrow \quad \hat{C} = \begin{bmatrix} s_1^2 & \sqrt{s_1 s_2} e^{j(\phi_1 - \phi_2)} & \dots & \sqrt{s_1 s_m} e^{j(\phi_1 - \phi_m)} \\ \sqrt{s_1 s_2} e^{j(\phi_2 - \phi_1)} & s_2^2 & \dots & \sqrt{s_2 s_m} e^{j(\phi_2 - \phi_m)} \\ \vdots & \vdots & \ddots & \vdots \\ \sqrt{s_1 s_m} e^{j(\phi_m - \phi_1)} & \sqrt{s_2 s_m} e^{j(\phi_m - \phi_2)} & \dots & s_m^2 \end{bmatrix} \begin{bmatrix} 1 & 0 & \dots & 0 \\ 0 & 1 & \dots & 0 \\ \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & \dots & 1 \end{bmatrix}$$

Multidimensional extension

- Extension only possible for the extreme case  $E\{nn^H\} = \mathbf{I}_{m \times m}$  as data's correlation is not considered



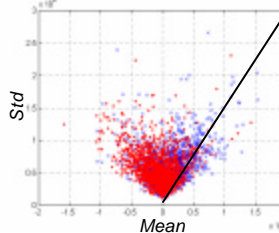
Grass area  
Statistics calculated over 7x7 pixel windows



Copolar

Blue:  $\text{Real}(S_{hh} S_{vv}^*)$   
Red:  $\text{Imag}(S_{hh} S_{vv}^*)$

$$|r_{hhvv}| = 0.77 e^{j0.807}$$



Crosspolar

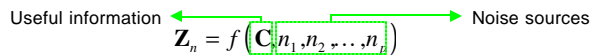
Blue:  $\text{Real}(S_{hh} S_{hv}^*)$   
Red:  $\text{Imag}(S_{hh} S_{hv}^*)$

$$|r_{hhvv}| = 0.118 e^{j0.638}$$

$S_{hh}$  amplitude  
E-SAR L-band system



### Objective of a multidimensional speckle noise model



- Overcome the limitations of the fully multiplicative speckle noise model. Noise model independent of the data dimensionality and valid for any correlation structure for the data
  - Observation: Any matrix entry consists of the Hermitian product of two complex SAR images

One-look sample covariance matrix  $\mathbf{Z}_1 = \mathbf{k}\mathbf{k}^H = \begin{bmatrix} S_1 S_1^H & S_1 S_2^H & \cdots & S_1 S_m^H \\ S_2 S_1^H & S_2 S_2^H & \cdots & S_2 S_m^H \\ \vdots & \vdots & \ddots & \vdots \\ S_m S_1^H & S_m S_2^H & \cdots & S_m S_m^H \end{bmatrix}$

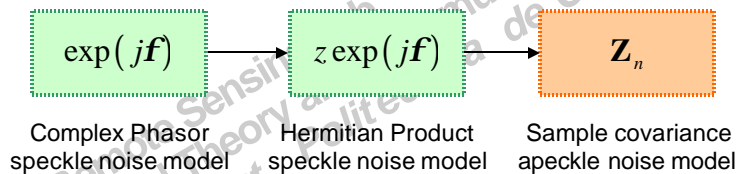
- Speckle noise model for the Hermitian product of a pair of SAR images



Extension to model the sample covariance matrix independently of its dimensions



### Procedure to derive the multidimensional speckle noise model



Complex Phasor speckle noise model      Hermitian Product speckle noise model      Sample covariance speckle noise model

Multidimensional SAR Speckle Models **Complex Phasor Speckle Noise Model**

$\exp(j\phi) \rightarrow z \exp(j\phi) \rightarrow [Z]$

- Phase distribution under the **Gaussian Scattering Assumption**

$$p_r(f) = \frac{\Gamma(n+1/2)(1-|r|^2)^n}{2\sqrt{\rho}\Gamma(n)(1-b^2)^{n+1/2}} \frac{(1-|r|^2)^n}{2p} {}_2F_1\left(n, 1; \frac{1}{2}; b^2\right) \quad b = |r| \cos(f-f_c)$$
- Phase additive noise model
 
$$\phi = \phi_x + v \quad [\phi_x - \pi, \phi_x + \pi]$$

$$E\{\phi\} = \phi_x$$

$$\text{var}\{v\} = f(|\rho|)$$
- Useful signal separation from noise component under the complex phasor formulation
 
$$e^{j\phi} = \Re\{e^{j\phi}\} + j\Im\{e^{j\phi}\} = \cos(\phi) + j \sin(\phi) \quad \begin{cases} \cos(\phi) = \cos(\phi_x) \cos(v) - \sin(\phi_x) \sin(v) \\ \sin(\phi) = \cos(\phi_x) \sin(v) + \sin(\phi_x) \cos(v) \end{cases}$$

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Multidimensional SAR Speckle Models **Complex Phasor Speckle Noise Model**

- Interferometric phase noise real part
 
$$\cos(v) = N_c + v'_1$$

$$N_c = E\{\cos(v)\} = \frac{\pi}{4} |\rho| {}_2F_1\left(\frac{1}{2}, \frac{1}{2}; 2; |\rho|^2\right)$$

$$E\{v'_1\} = 0 \quad \sigma_{v'_1}^2 = \frac{1}{2}(1 - |\rho|^2)^{0.79}$$
- Interferometric phase noise imaginary part
 
$$\sin(v) = v'_2$$

$$E\{v'_2\} = 0 \quad \sigma_{v'_2}^2 = \frac{1}{2}(1 - |\rho|^2)^{0.58}$$
- Information location within the complex phasor
 
$$\begin{aligned} \cos(\phi) &= N_c \cos(\phi_x) + v'_1 \cos(\phi_x) - v'_2 \sin(\phi_x) \\ \sin(\phi) &= N_c \sin(\phi_x) + v'_1 \sin(\phi_x) + v'_2 \cos(\phi_x) \end{aligned}$$

$N_c$  considered as signal component      Noise terms. Phase information is lost

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Multidimensional  
SAR Speckle Models

## Complex Phasor Speckle Noise Model

- Combination of the additive noise terms  $v'_1$  and  $v'_2$

$$v_c = v'_1 \cos(\phi_x) - v'_2 \sin(\phi_x)$$

$$v_s = v'_1 \sin(\phi_x) + v'_2 \cos(\phi_x)$$

$$E\{v_c\} = E\{v_s\} = 0$$

$$\sigma_{v_c}^2 = \sigma_{v'_1}^2 \cos^2(\phi_x) + \sigma_{v'_2}^2 \sin^2(\phi_x)$$

$$\sigma_{v_s}^2 = \sigma_{v'_1}^2 \sin^2(\phi_x) + \sigma_{v'_2}^2 \cos^2(\phi_x)$$

$$\sigma_{v_c}^2 = \sigma_{v_s}^2 = \frac{1}{2}(1 - |\rho|^2)0.685$$

■ Interferometric phasor noise model

$$e^{j\mathbf{f}} = \underbrace{N_c e^{j\mathbf{f}_x}}_{\text{Multiplicative component}} + \underbrace{(v_c + jv_s)}_{\text{Additive component}}$$

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Multidimensional  
SAR Speckle Models

## Hermitian Product Speckle Noise Model

$\exp(j\phi) \longrightarrow \boxed{z \exp(j\phi)} \longrightarrow [Z]$

Extended complex phasor

$$\exp(j\phi) \begin{cases} \cos(\phi) = N_c \cos(\phi_x) + v'_1 \cos(\phi_x) - v'_2 \sin(\phi_x) \\ \sin(\phi) = N_c \sin(\phi_x) + v'_1 \sin(\phi_x) + v'_2 \cos(\phi_x) \end{cases}$$

- Complex Hermitian product speckle noise model as extension of the complex phasor speckle noise model

$$S_k S_l^* = |S_k S_l^*| e^{j(\theta_k - \theta_l)} = z e^{j\phi}$$

$$\Re\{z e^{j\phi}\} = N_c z \cos(\phi_x) + z v'_1 \cos(\phi_x) - z v'_2 \sin(\phi_x)$$

$$\Im\{z e^{j\phi}\} = N_c z \sin(\phi_x) + z v'_1 \sin(\phi_x) + z v'_2 \cos(\phi_x)$$

$$\boxed{z e^{j\mathbf{f}} = [z N_c + (z v'_1 + j z v'_2)] \exp(j \mathbf{f}_x)}$$

- The phase  $\phi_x$  is considered as the average phase difference in the case of homogeneous data
- Identification of noise sources in each additive element by considering homogeneous data

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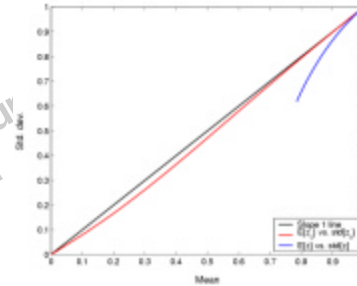
$$ze^{j\phi} = [zN_c + (zv'_1 + jzv'_2)] \exp(j\phi_x)$$

- Random behaviour determined by the amplitude  $z$

$$\begin{aligned} \Re\{ze^{j\phi}\}_1 &= zN_c \cos(\phi_x) \\ \Im\{ze^{j\phi}\}_1 &= zN_c \sin(\phi_x) \end{aligned}$$

- $N_c$  determines the final properties of this additive component as it depends also on the coherence  $|\rho|$

$$\begin{aligned} E\{\Re\{ze^{j\phi}\}_1\} &= \psi N_c \frac{\pi}{4} {}_2F_1\left(-\frac{1}{2}, -\frac{1}{2}; 1; |\rho|^2\right) \cos(\phi_x) \\ \text{var}\{\Re\{ze^{j\phi}\}_1\} &= \psi^2 N_c^2 \left(1 + |\rho|^2 - \left(\frac{\pi}{4}\right)^2 {}_2F_1\left(-\frac{1}{2}, -\frac{1}{2}; 1; |\rho|^2\right)\right) \cos^2(\phi_x) \\ \text{std}\{\Re\{ze^{j\phi}\}_1\} &\simeq \text{abs}\left(E\{\Re\{ze^{j\phi}\}_1\}\right) \end{aligned}$$



$$\{ze^{j\phi}\}_1 = \psi N_c \bar{z}_n n_m e^{j\phi_x}$$

$$\begin{aligned} E\{n_m\} &= 1 \\ \text{var}\{n_m\} &= 1 \end{aligned}$$

**Multiplicative noise behaviour**



$$ze^{j\phi} = [zN_c + (zv'_1 + jzv'_2)] \exp(j\phi_x)$$

- Random component determined by  $z$  and the phase noise term  $v'_1$

$$\begin{aligned} \Re\{ze^{j\phi}\}_2 &= zv'_1 \cos(\phi_x) \\ \Im\{ze^{j\phi}\}_2 &= zv'_1 \sin(\phi_x) \end{aligned}$$

$$\begin{aligned} E\{\Re\{ze^{j\phi}\}_2\} &= \psi \left(|\rho| - N_c \frac{\pi}{4} {}_2F_1\left(-\frac{1}{2}, -\frac{1}{2}; 1; |\rho|^2\right)\right) \cos(\phi_x) \\ \text{var}\{\Re\{ze^{j\phi}\}_2\} &\simeq \frac{1}{2} \psi^2 (1 - |\rho|^2)^{1.64} \cos^2(\phi_x) \end{aligned}$$

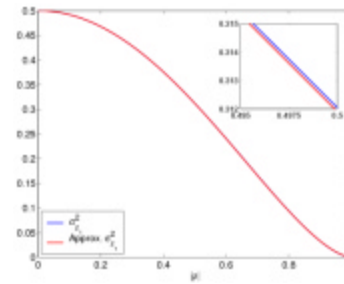
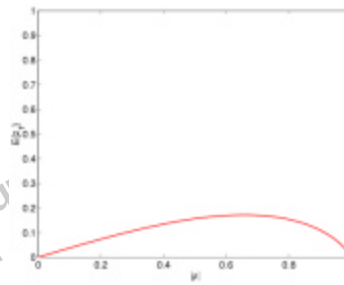
- The mean and the variance depend differently on the coherence  $|\rho|$

$$\{ze^{j\phi}\}_2 = \psi [ (|\rho| - N_c \bar{z}_n) + n_{a1} ] e^{j\phi_x}$$

$$\begin{aligned} E\{n_{a1}\} &= 0 \\ \text{var}\{n_{a1}\} &= \frac{1}{2} (1 - |\rho|^2)^{1.64} \end{aligned}$$



**Additive noise behaviour**





$$ze^{j\phi} = [zN_c + (zv'_1 + jzv'_2)] \exp(j\phi_x)$$

- Random component determined by  $z$  and the phase noise term  $v'_2$

$$\Re\{ze^{j\phi}\}_3 = -zv'_2 \sin(\phi_x)$$

$$\Im\{ze^{j\phi}\}_3 = zv'_2 \cos(\phi_x)$$

$$E\{\Re\{ze^{j\phi}\}_3\} = 0$$

$$\text{var}\{\Re\{ze^{j\phi}\}_3\} = \frac{1}{2}\psi^2(1 - |\rho|^2)\sin^2(\phi_x)$$

$$\{ze^{j\phi}\}_3 = j\psi n_{a2}e^{j\phi_x}$$

$$E\{n_{a2}\} = 0$$

$$\text{var}\{n_{a2}\} = \frac{1}{2}(1 - |\rho|^2)$$

Additive noise behaviour

- Complex Hermitian product speckle noise model

$$S_k S_l^* = f(\psi|\rho| \exp(j\phi_x), [n_m, n_{ar}, n_{ai}]^T)$$

$$S_k S_l^* = ze^{j\phi} = \{ze^{j\phi}\}_1 + \{ze^{j\phi}\}_2 + \{ze^{j\phi}\}_3$$

$$= \psi N_c \bar{z}_n n_m e^{j\phi_x} + \psi [ (|\rho| - N_c \bar{z}_n) + n_{a1} ] e^{j\phi_x} + j\psi n_{a2} e^{j\phi_x}$$

$$C_{n_m n_{a1}} \neq 0$$

$$C_{n_m n_{a2}} = 0$$

$$C_{n_{a1} n_{a2}} = 0$$



- Combination of the additive noise terms  $n_{ar}$  and  $n_{ai}$

$$\psi n_{ar} = \psi n_{a1} \cos(\phi_x) - \psi n_{a2} \sin(\phi_x)$$

$$\psi n_{ai} = \psi n_{a1} \sin(\phi_x) + \psi n_{a2} \cos(\phi_x)$$

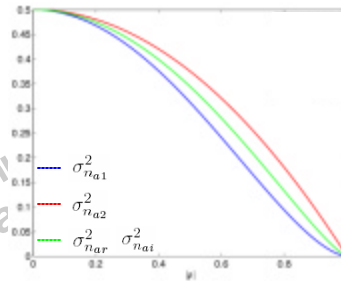
$$E\{n_{ar}\} = E\{n_{a1}\} \cos(\phi_x) - E\{n_{a2}\} \sin(\phi_x) = 0$$

$$E\{n_{ai}\} = E\{n_{a1}\} \sin(\phi_x) + E\{n_{a2}\} \cos(\phi_x) = 0$$

$$\sigma_{n_{ar}}^2 = \sigma_{n_{a1}}^2 \cos^2(\phi_x) + \sigma_{n_{a2}}^2 \sin^2(\phi_x)$$

$$\sigma_{n_{ai}}^2 = \sigma_{n_{a1}}^2 \sin^2(\phi_x) + \sigma_{n_{a2}}^2 \cos^2(\phi_x)$$

$$\sigma_{n_{ar}}^2 = \sigma_{n_{ai}}^2 = \frac{1}{2}(1 - |\rho|^2)^{1.32}$$

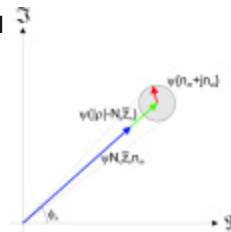


- Complex Hermitian product linear speckle noise model

$$S_k S_l^* = \mathbf{y} N_c \bar{z}_n n_m e^{j\phi_x} + \mathbf{y} (|\mathbf{r}| - N_c \bar{z}_n) e^{j\phi_x} + \mathbf{y} (n_{ar} + jn_{ai})$$

Multiplicative term

Additive term





$$S_k S_l^* = \mathbf{y} N_c \bar{z}_n n_m e^{j\phi_x} + \mathbf{y} (|\mathbf{r}| - N_c \bar{z}_n) e^{j\phi_x} + \mathbf{y} (n_{ar} + j n_{ai})$$

Multiplicative speckle component:  $n_m$  → High coherence areas  
 Stationary

$$\Re\{z e^{j\phi}\}_1 = z_c \cos(\phi_x) = \psi N_c \bar{z}_n n_m \cos(\phi_x)$$

$$\Im\{z e^{j\phi}\}_1 = z_c \sin(\phi_x) = \psi N_c \bar{z}_n n_m \sin(\phi_x)$$

$$N_c \bar{z}_n \sigma_{n_m} = \sigma_{n_{ar}} = \sigma_{n_{ai}} \\ |\rho| = 0.675$$

Additive speckle components:  $n_{ar}, n_{ai}$  → Low coherence areas  
 Non stationary

Final speckle noise behaviour { Combination of multiplicative and additive noise components, determined by  $\rho$

### Special cases

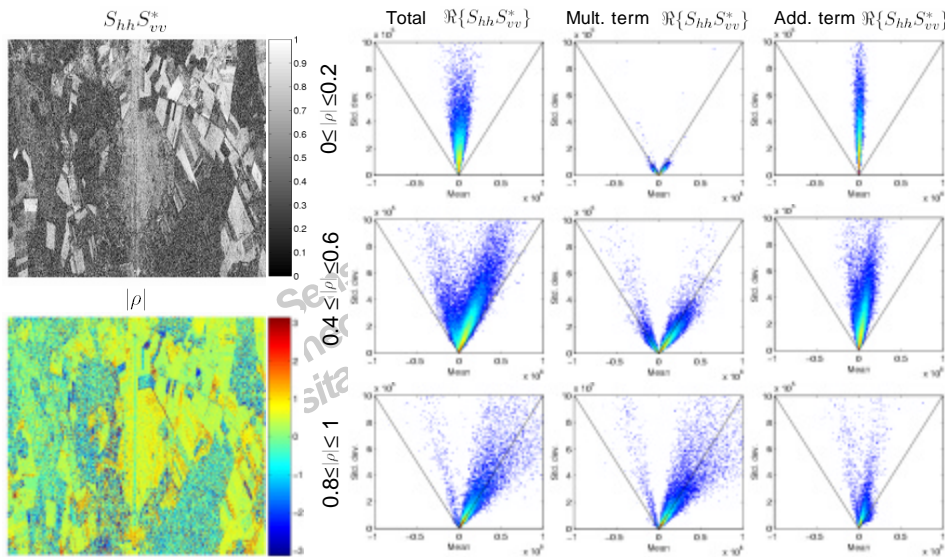
- Covariance matrix diagonal element

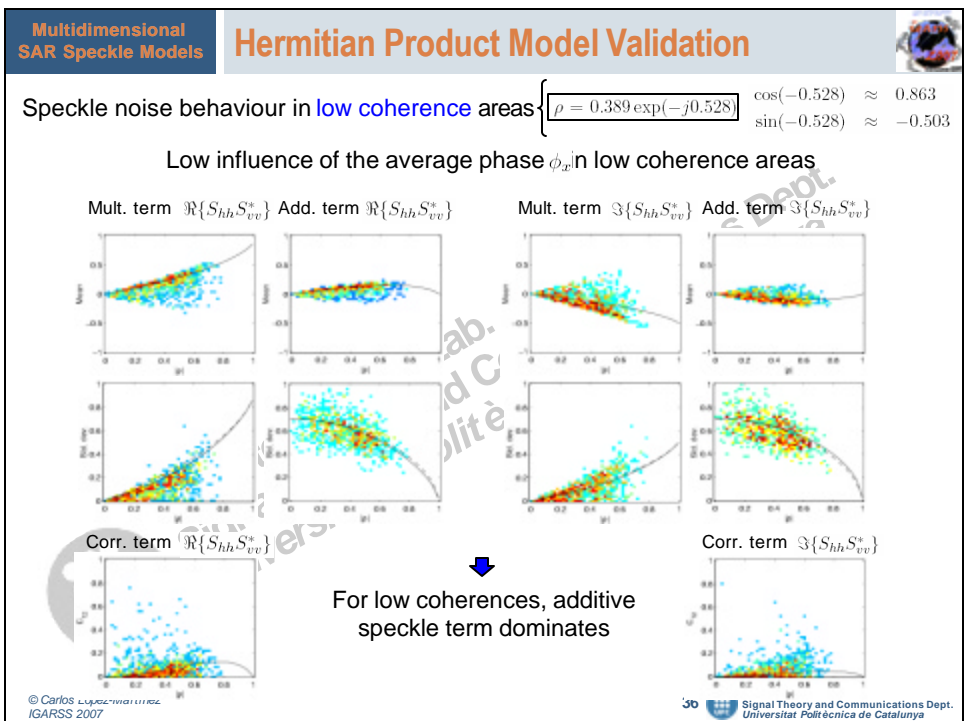
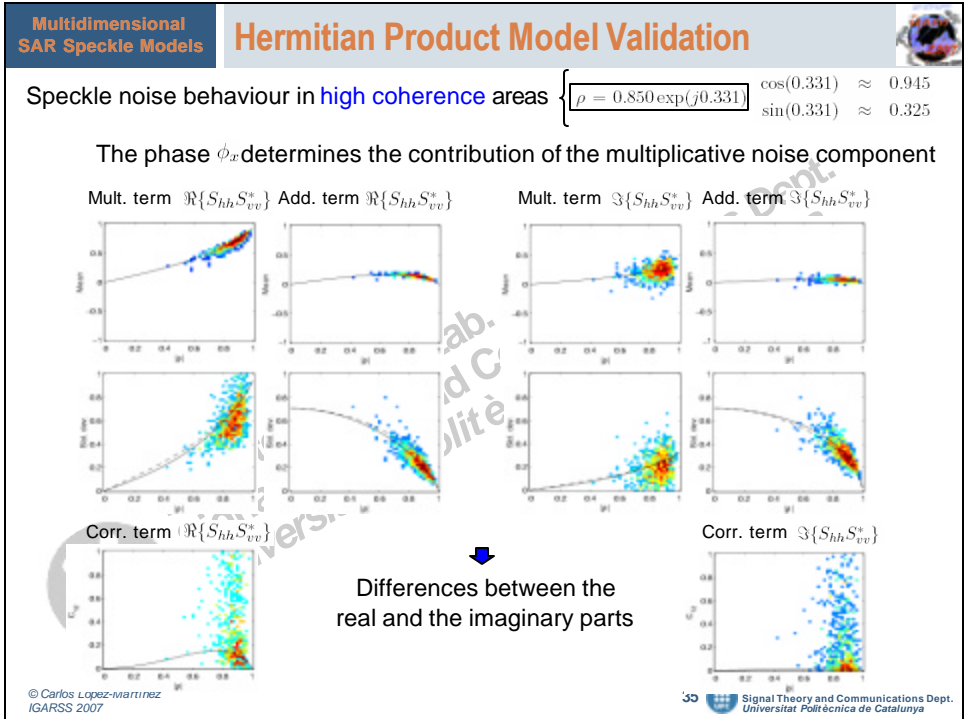
$$\rho = 1 \exp(j0) \rightarrow S_k S_k^* = \psi n_m$$

- By construction, the complex Hermitian product phase difference is characterized by an additive noise model



L-band (1.3 GHz) fully PolSAR data. E-SAR system. Oberpfaffenhofen test area (D)







Extension of the Hermitian Product Speckle Noise Model

**Gaussian hypothesis**  $\left\{ \begin{array}{l} E\{\mathbf{Z}_n\} = E\{Q(\mathbf{Z}_n)\} \rightarrow f(\mathbf{C}) \\ Q(\mathbf{Z}_n) \text{ Polynomial depending on the entries of } \mathbf{Z}_n \text{, invariant in the sense that it only depends on the eigenvalues of } \mathbf{Z}_n \end{array} \right.$

G. Letac and H. Massam, "All Invariant Moments of the Wishart Distribution", Scand. J. of Statistics, vol. 31, no. 2, pp.295-318, June 2004

- Rearrangement of the Hermitian product speckle noise model
- $$\langle S_k S_l^* \rangle_n = \mathbf{y} n_m \exp(j\mathbf{f}_x) + \mathbf{y} (\mathbf{r} | - N_c \bar{z}_n) \exp(j\mathbf{f}_x) + \mathbf{y} (n_{ar} + jn_{ai}) \quad k, l = 1, 2, \dots, m.$$

$$\langle S_k S_l^* \rangle_n = \mathbf{y} | \mathbf{r} | \exp(j\mathbf{f}_x) + \mathbf{y} (n_m - N_c \bar{z}_n) \exp(j\mathbf{f}_x) + \mathbf{y} (n_{ar} + jn_{ai}) \quad k, l = 1, 2, \dots, m$$

- Matrix speckle noise model
- $$\mathbf{Z}_n = \mathbf{C} + \mathbf{N}_{ij} + \mathbf{N}_{ij}^*$$
- $$\left\{ \begin{array}{l} N_{mji} = n_{mii} \\ N_{mij} = \mathbf{y}_{ij} (n_{mij} - N_{cij} \bar{z}_{n,ij}) \exp(j\mathbf{f}_{xij}) \\ N_{aii} = 0 \\ N_{aij} = \mathbf{y}_{ij} (n_{arj} + jn_{aij}) \end{array} \right.$$

- Coherent with previous results in the literature (Perturbation analysis)
- $$\langle \mathbf{k} \mathbf{k}^* \rangle = \mathbf{C} + ?$$
- H. Krim, P. Forster, J.G. Proakis, "Operator approach to performance analysis of root-MUSIC and rootmin-norm" IEEE Trans. Signal Processing, vol.40, no. 7, pp. 1687- 1696, July 1992



A multidimensional SAR data speckle noise model for **already multilooked data**

- Sometimes, depending on the SAR sensor, only multilook data is available

$$\mathbf{Z}_n = \frac{1}{n} \sum_{k=1}^n \mathbf{k} \mathbf{k}^H = \begin{bmatrix} \frac{1}{n} \sum_{k=1}^n S_1(k) S_1^*(k) & \frac{1}{n} \sum_{k=1}^n S_1(k) S_2^*(k) & \dots & \frac{1}{n} \sum_{k=1}^n S_1(k) S_m^*(k) \\ \frac{1}{n} \sum_{k=1}^n S_2(k) S_1^*(k) & \frac{1}{n} \sum_{k=1}^n S_2(k) S_2^*(k) & \dots & \frac{1}{n} \sum_{k=1}^n S_2(k) S_m^*(k) \\ \vdots & \vdots & \ddots & \vdots \\ \frac{1}{n} \sum_{k=1}^n S_m(k) S_1^*(k) & \frac{1}{n} \sum_{k=1}^n S_m(k) S_2^*(k) & \dots & \frac{1}{n} \sum_{k=1}^n S_m(k) S_m^*(k) \end{bmatrix}$$



The Hermitian product phase difference pdf

$$\langle S_i S_j^* \rangle_n = z \exp(j\mathbf{f}) \quad i, j = 1, 2, \dots, m \quad p_r(\mathbf{f}) = \frac{\Gamma(n+1/2)(1-|\mathbf{r}|^2)^n \mathbf{b} + (1-|\mathbf{r}|^2)^n}{2\sqrt{p}\Gamma(n)(1-\mathbf{b}^2)^{n+1/2}} {}_2F_1\left(n, 1; \frac{1}{2}; \mathbf{b}^2\right)$$

Phase difference model  $\rightarrow \mathbf{f} = \mathbf{f}_x + \mathbf{v}$  still valid

$$\Re\{\exp(j\mathbf{f})\} = N_c \cos(\mathbf{f}_x) + v'_1 \cos(\mathbf{f}_x) - v'_2 \sin(\mathbf{f}_x)$$

$$\Im\{\exp(j\mathbf{f})\} = N_c \sin(\mathbf{f}_x) + v'_1 \sin(\mathbf{f}_x) + v'_2 \cos(\mathbf{f}_x)$$

$$\exp(j\mathbf{f}) = N_c \exp(j\mathbf{f}_x) + (v'_1 + jv'_2)$$

Amplitude information

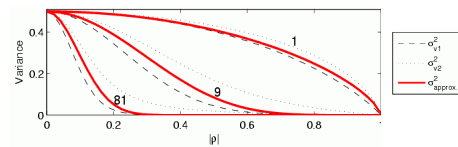
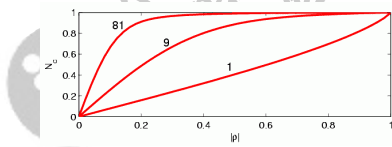
$$N_c = \frac{\Gamma(n+1/2)\Gamma(3/2)}{\Gamma(n)} |\mathbf{r}| {}_2F_1\left(\frac{3}{2}, n, \frac{1}{2}; 2; |\mathbf{r}|^2\right)$$

Noise components

$$E\{v'_i\} = E\{v'_s\} = 0$$

$$\mathbf{s}_v^2 = \mathbf{s}_{v'_s}^2 = \frac{1}{2}(1-|\mathbf{r}|^2)^{2n}$$

$$a = 0.685$$



$$\langle S_i S_j^* \rangle_n = z \exp(j\mathbf{f}) \quad i, j = 1, 2, \dots, m$$

$$\Re\{z \exp(j\mathbf{f})\} = z N_c \cos(\mathbf{f}_x) + z v'_1 \cos(\mathbf{f}_x) - z v'_2 \sin(\mathbf{f}_x)$$

$$\Im\{z \exp(j\mathbf{f})\} = z N_c \sin(\mathbf{f}_x) + z v'_1 \sin(\mathbf{f}_x) + z v'_2 \cos(\mathbf{f}_x)$$

Single-look data

$$z N_c \exp(j\mathbf{f}_x) = \mathbf{y} \exp(j\mathbf{f}_x) \bar{z}_n N_c n_m$$

$$E\{n_m\} = 1$$

$$\mathbf{s}_{n_m}^2 = 1$$

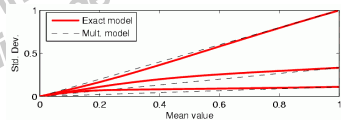
Multilook data

Extension of the single-look model NOT possible

$$z N_c \exp(j\mathbf{f}_x) = \mathbf{y} \exp(j\mathbf{f}_x) n_m$$

$$E\{n_m\} = N_c \bar{z}_n \quad (\text{Exact value})$$

$$\text{var}\{n_m\} = N_c^2 \frac{(1+|\mathbf{r}|^2)}{2n} \quad (1^{\text{st}} \text{ order approx.})$$



Asymptotic analysis: Mean values are exact. Std dev. are approximated

$$\lim_{n \rightarrow \infty} E\{z N_c \cos(\mathbf{f}_x)\} = \mathbf{y} |\mathbf{r}| \cos(\mathbf{f}_x) \quad \lim_{n \rightarrow \infty} \mathbf{s}_{z N_c \cos(\mathbf{f}_x)}^2 = 0$$

$$\lim_{n \rightarrow \infty} E\{z N_c \sin(\mathbf{f}_x)\} = \mathbf{y} |\mathbf{r}| \sin(\mathbf{f}_x) \quad \lim_{n \rightarrow \infty} \mathbf{s}_{z N_c \sin(\mathbf{f}_x)}^2 = 0$$

• No loss of information

• All information contained in the first additive term as  $n \rightarrow \infty$



$$\langle S_i, S_j \rangle_n = z \exp(jf) \quad i, j = 1, 2, \dots, m$$

$$\Re\{z \exp(jf)\} = z N_c \cos(f_x) + z v'_1 \cos(f_x) - z v'_2 \sin(f_x)$$

$$\Im\{z \exp(jf)\} = z N_c \sin(f_x) + z v'_1 \sin(f_x) + z v'_2 \cos(f_x)$$

Single-look data

$$z v'_1 \exp(jf_x) = y \{(|r| - N_c \bar{z}_n) + n_{a1}\} \exp(jf_x)$$

$$E\{n_{a1}\} = 0$$

$$s_{n_{a1}}^2 \approx \frac{1}{2} (1 - |r|^2)^{1.64}$$

Multilook data

Extension of the single-look model POSSIBLE

$$z v'_1 \exp(jf_x) = y \{(|r| - N_c \bar{z}_n) + n_{a1}\} \exp(jf_x)$$

$$E\{n_{a1}\} = 0 \quad (\text{Exact value})$$

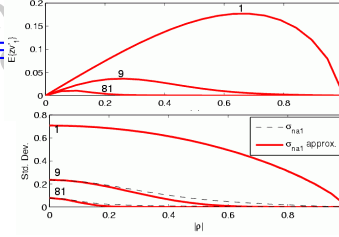
$$s_{n_{a1}}^2 \approx \frac{1}{2n} (1 - |r|^2)^{1.64n} \quad (\text{Approx.})$$

Asymptotic analysis

$$\lim_{n \rightarrow \infty} E\{z v'_1 \cos(f_x)\} = 0 \quad \lim_{n \rightarrow \infty} \text{var}\{z v'_1 \cos(f_x)\} = 0$$

$$\lim_{n \rightarrow \infty} E\{z v'_1 \sin(f_x)\} = 0 \quad \lim_{n \rightarrow \infty} \text{var}\{z v'_1 \sin(f_x)\} = 0$$

- No loss of information



$$\langle S_i, S_j \rangle_n = z \exp(jf) \quad i, j = 1, 2, \dots, m$$

$$\Re\{z \exp(jf)\} = z N_c \cos(f_x) + z v'_1 \cos(f_x) - z v'_2 \sin(f_x)$$

$$\Im\{z \exp(jf)\} = z N_c \sin(f_x) + z v'_1 \sin(f_x) + z v'_2 \cos(f_x)$$

Single-look data

$$z v'_2 \exp(jf_x) = y n_{a2} \exp(jf_x)$$

$$E\{n_{a2}\} = 0$$

$$s_{n_{a2}}^2 = \frac{1}{2n} (1 - |r|^2)$$

Multilook data

Extension of the single-look model POSSIBLE

$$z v'_2 \exp(jf_x) = y n_{a2} \exp(jf_x)$$

$$E\{n_{a2}\} = 0 \quad (\text{Exact value})$$

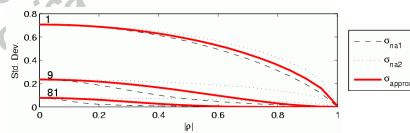
$$s_{n_{a2}}^2 = \frac{1}{2n} (1 - |r|^2) \quad (\text{Exact value})$$

Unification of the additive noise terms

$$n_{ar} = n_{a1} \cos(f_x) - n_{a2} \sin(f_x)$$

$$n_{ai} = n_{a1} \sin(f_x) + n_{a2} \cos(f_x)$$

$$E\{n_{ar}\} = E\{n_{ai}\} = 0 \quad s_{n_{ar}}^2 = s_{n_{ai}}^2 \approx \frac{1}{2n} (1 - |r|^2)^{1.32\sqrt{n}} \quad (\text{Approx.})$$





Multidimensional SAR Speckle Models

## Multidimensional Multilook Speckle Model

$$\langle S_i S_j^* \rangle_n = z \exp(jf) \quad i, j = 1, 2, \dots, m$$

↓

$$\langle S_i S_j^* \rangle_n = y n_m \exp(jf_x) + y (|r| - N_c \bar{z}_n) \exp(jf_x) + y (n_{ar} + j n_{ai}) \quad i, j = 1, 2, \dots, m$$

- Multiplicative speckle noise component
  - Dominant for **high** coherences
  - Modulated by phase information

$$E\{n_m\} = N_c \bar{z}_n \quad s_{n_m}^2 = N_c^2 \frac{(1+|r|^2)}{2n}$$

- Additive speckle noise component
  - Dominant for **low** coherences
  - Not affected by phase information

$$E\{n_{ar}\} = E\{n_{ai}\} = 0 \quad s_{n_{ar}}^2 = s_{n_{ai}}^2 = \frac{1}{2n} (1-|r|^2)^{1.32} \sqrt{r}$$

- Effect of the approximations
  - Mean value **IS NOT** approximated → No loss of information

$$\lim_{n \rightarrow \infty} \{y n_m \exp(jf_x) + y (|r| - N_c \bar{z}_n) \exp(jf_x) + y (n_{ar} + j n_{ai})\} = y |r| \exp(jf_x)$$

- Std. Dev. **ARE** approximated

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Multidimensional SAR Speckle Models

## Multidimensional Multilook Speckle Model Validation

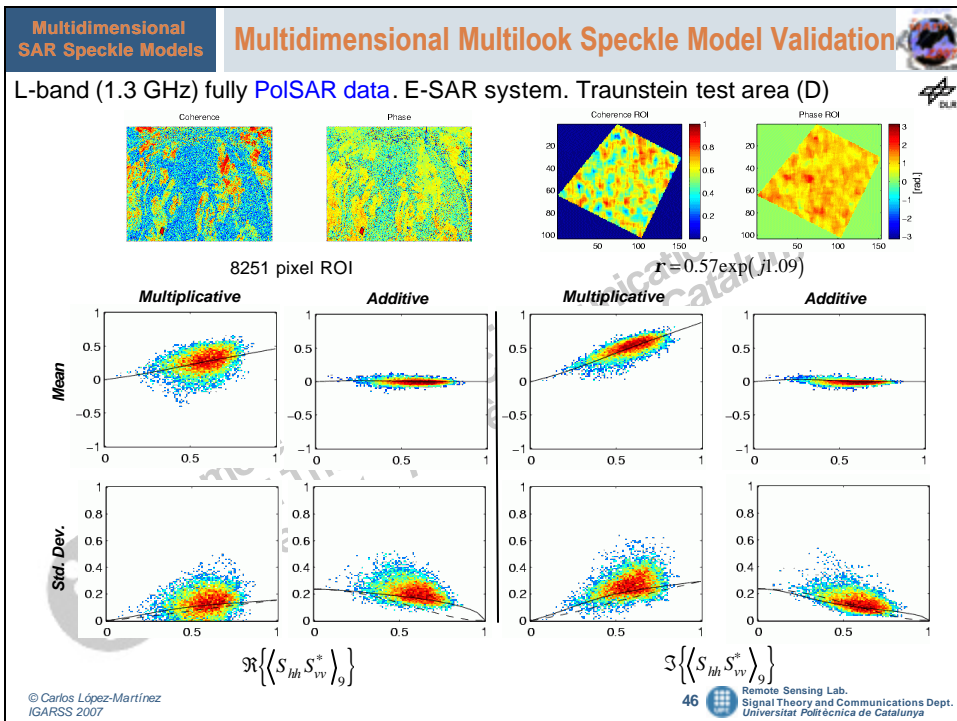
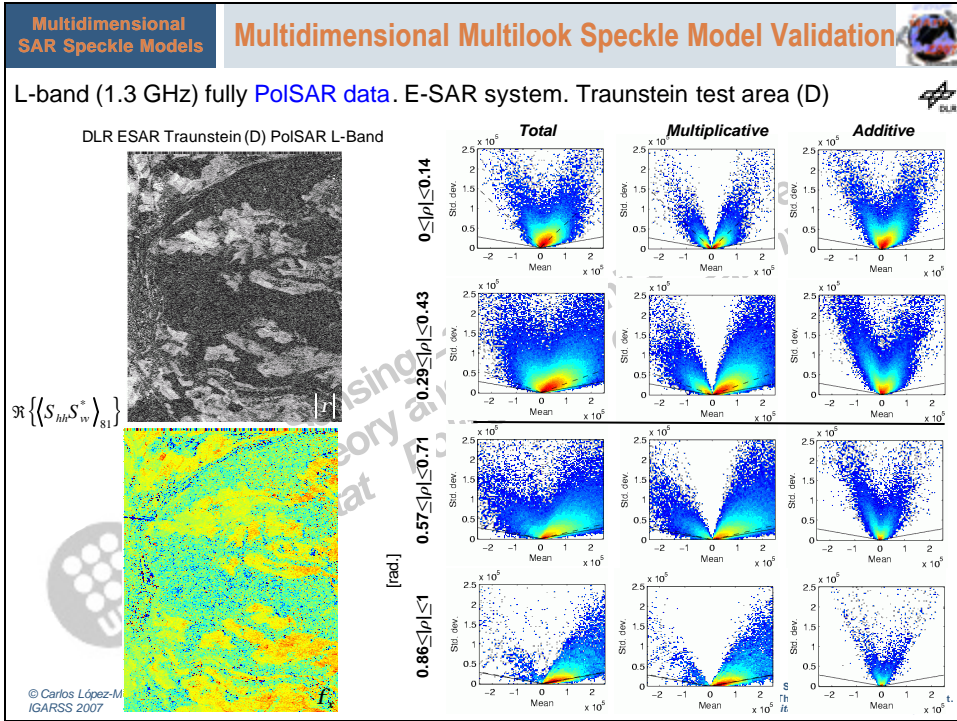
L-band (1.3 GHz) fully PolSAR data. E-SAR system. Traunstein test area (D)

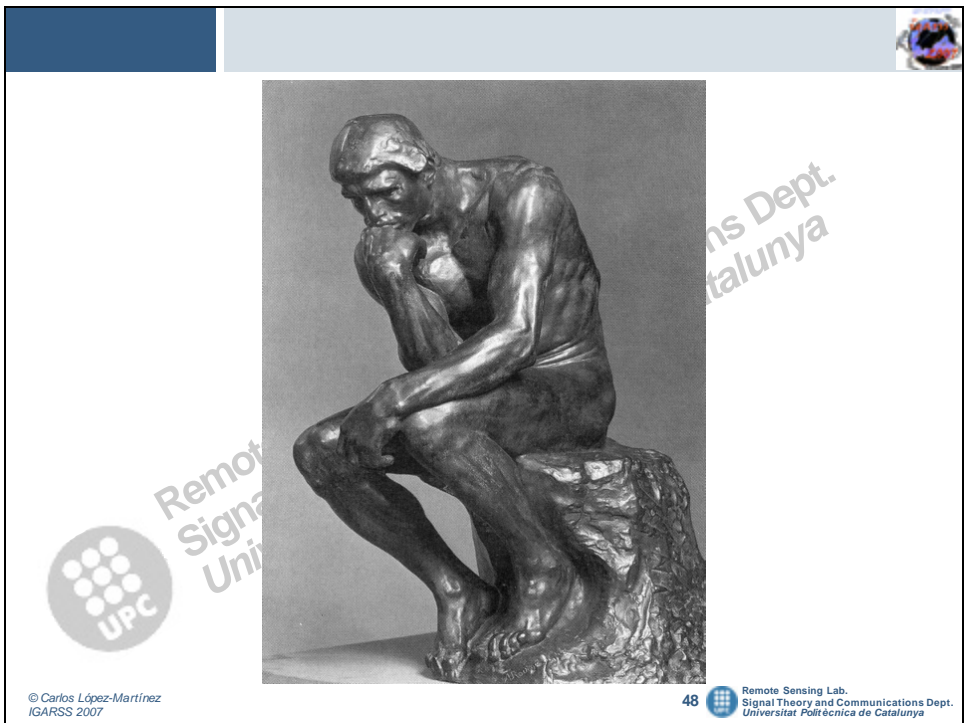
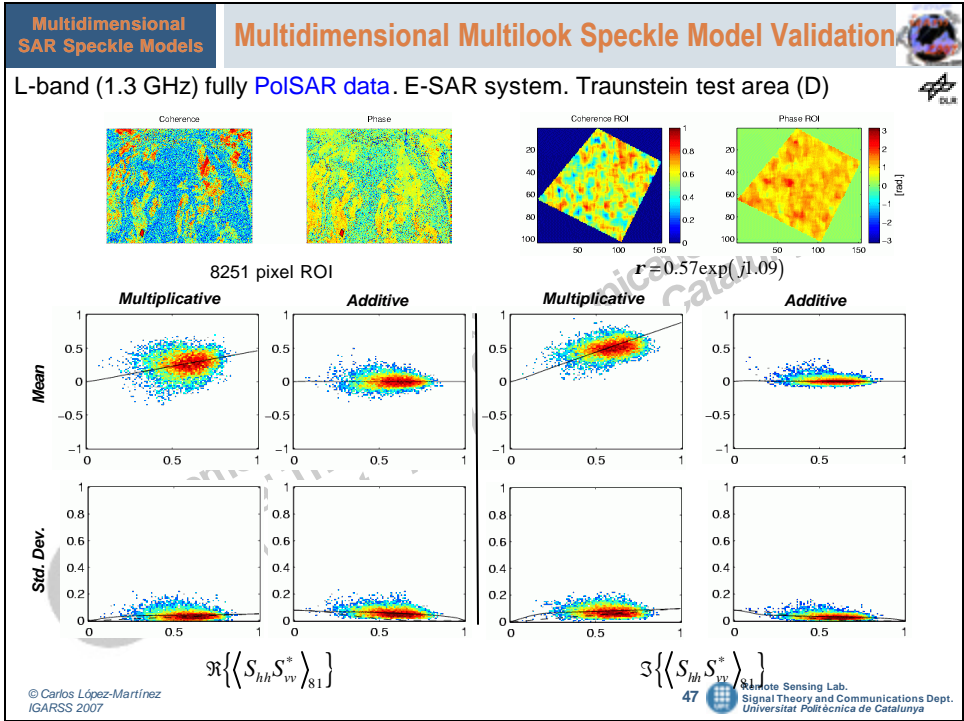
DLR ESAR Traunstein (D) PolSAR L-Band

$\Re\{S_{hh} S_{vv}^*\}_9$

	Total	Multiplicative	Additive
$0 \leq  \rho  \leq 0.14$			
$0.29 \leq  \rho  \leq 0.43$			
$0.57 \leq  \rho  \leq 0.71$			
$0.86 \leq  \rho  \leq 1$			

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## Coherence Estimation

SAR Single-Channel and Multi-Channel complex correlation

- Useful information contained in the Hermitian product (second order moment) of the pairs of SAR images

Complex correlation coefficient  $r = \frac{E\{S_1 S_2^*\}}{\sqrt{E\{|S_1|^2\} E\{|S_2|^2\}}} = \boxed{r} e^{j\phi}$  → Coherence

- Coherence estimation through multilook techniques

Multilook techniques  $|\hat{r}_{MLT}| = \frac{|\sum_{m=1}^M \sum_{n=1}^N S_1(m, n) S_2^*(m, n)|}{\sqrt{\sum_{m=1}^M \sum_{n=1}^N |S_1(m, n)|^2 \sum_{m=1}^M \sum_{n=1}^N |S_2(m, n)|^2}}$

- Overestimation for low coherence values
- Bias due to systematic phase variations
- Origin?, Quantification?, Reduction/Elimination?

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**Coherence Estimation** **Topographic Effects**

Effects of **topography** in coherence estimation

- Coherence estimated in a 5x5-pixel window

40-pixel fringes

12-pixel fringes

Steep topography induces coherence bias

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**Coherence Estimation** **Speckle Bias**

Effects of **number of samples (looks)** employed to estimate coherence

9 looks

25 looks

49 looks

81 looks

- Multilook coherence is as asymptotically non-biased coherence estimator.

Looks ↗ ⇨ Coherence bias ↘

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## Modelling of the Interferometric Coherence Parameter: Topographic Effects

Systematic phase variations corrupt coherence estimation since the hypothesis of data homogeneity is not valid

Introduction of topographic effects in the speckle model of  $S_1 S_2^*$

$$S_1 S_2^* = \mathbf{y} \bar{z}_n n_m N e^{j f_x} + \mathbf{y} (|\mathbf{r}| - N_c \bar{z}_n) e^{j f_x} + \mathbf{y} (n_{ar} + j n_{ai})$$

Hypothesis: Topography model  $\Rightarrow$  2D separable slope

$$f_x(m, n) = \frac{2p}{S_x} m + \frac{2p}{S_y} n$$

Hypothesis: Multilook techniques to estimate coherence  $\Rightarrow$  Simplicity of analysis

$$h(m, n) = \frac{1}{MN} \sum_{p=1}^M \sum_{q=1}^N \mathbf{d}(m-p) \mathbf{d}(n-q)$$

$$H(\mathbf{w}_x, \mathbf{w}_y) = \frac{1}{M} \frac{\sin\left(\frac{M}{2} \mathbf{w}_x\right)}{\sin\left(\frac{\mathbf{w}_x}{2}\right)} \frac{1}{N} \frac{\sin\left(\frac{N}{2} \mathbf{w}_y\right)}{\sin\left(\frac{\mathbf{w}_y}{2}\right)}$$



The availability of the speckle noise model for  $S_1 S_2^*$  allows analyzing the effect of the multilook filter

$$x(m, n) = S_1 S_2^*(m, n) \rightarrow h(m, n) \rightarrow y(m, n) = (S_1 S_2^*)'(m, n)$$

Stochastic Analysis

$$S_{xx}(\mathbf{w}_x, \mathbf{w}_y) \rightarrow H(\mathbf{w}_x, \mathbf{w}_y) \rightarrow S_{yy}(\mathbf{w}_x, \mathbf{w}_y)$$

$$S_{yy}(\mathbf{w}_x, \mathbf{w}_y) = |H(\mathbf{w}_x, \mathbf{w}_y)|^2 S_{xx}(\mathbf{w}_x, \mathbf{w}_y)$$

Hypothesis: Uncorrelated speckle components

$$r_{n_m n_m}(k, l) = 1 + \mathbf{d}(k, l)$$

$$r_{n_{ar} n_{ar}}(k, l) = r_{n_{ai} n_{ai}}(k, l) = \frac{1}{2} (1 - |\mathbf{r}|^2)^{1.32} \mathbf{d}(k, l)$$

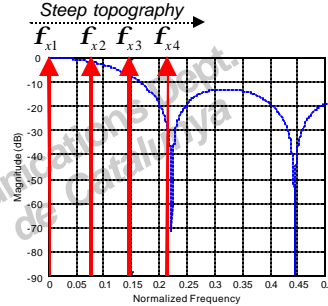


$$S_1 S_2^* = \mathbf{y} \bar{z}_n n_m N_c e^{j f_x} + \mathbf{y} (|\mathbf{r}| - N_c \bar{z}_n) e^{j f_x} + \mathbf{y} (n_{ar} + j n_{ai})$$

Spectral density function (*coherence information*) modulated by topography

$$S_{yy}(\mathbf{w}_x, \mathbf{w}_y) = |H(\mathbf{w}_x, \mathbf{w}_y)|^2 S_{xx}(\mathbf{w}_x, \mathbf{w}_y)$$

$$\Delta_{\text{topo}} = \left| \frac{1}{M} \frac{\sin\left(\frac{M}{2} \mathbf{w}_x\right)}{\sin\left(\frac{\mathbf{w}_x}{2}\right)} \frac{1}{N} \frac{\sin\left(\frac{N}{2} \mathbf{w}_y\right)}{\sin\left(\frac{\mathbf{w}_y}{2}\right)} \right|$$



$$\langle S_1 S_2^* \rangle_{MN} = \mathbf{y} \Delta_{\text{topo}} \bar{z}_n n_m' N_c e^{j f_x} + \mathbf{y} \Delta_{\text{topo}} (|\mathbf{r}| - N_c \bar{z}_n) e^{j f_x} + \mathbf{y} (n_{ar}' + j n_{ai}')$$

Quantification of the topographic bias (underestimates coherence)

Magnitude flat filters allow to estimate coherence independently from topography



Modelling of the complex correlation coefficient

$$r = \frac{E\{S_1 S_2^*\}}{\sqrt{E\{|S_1|^2\} E\{|S_2|^2\}}}$$

$$r = \frac{S_1 S_2^*}{\sqrt{|S_1|^2 |S_2|^2}}$$

Separate noise models for  $S_1$  and  $S_2$  *do not take into account* the correlation between SAR images

- Hypothesis: Independent modelling of  $S_1 S_2^*$  and  $S_1$  and  $S_2$

$$S_1 S_2^* = \mathbf{y} \bar{z}_n n_m N_c e^{j f_x} + \mathbf{y} (|\mathbf{r}| - N_c \bar{z}_n) e^{j f_x} + \mathbf{y} (n_{ar} + j n_{ai})$$

$$|S_1|^2 = \mathbf{s}_1 n_{m1}$$

$$|S_2|^2 = \mathbf{s}_2 n_{m2}$$

$$\Rightarrow |S_1|^2 |S_2|^2 = \mathbf{y} \sqrt{n_{m1} n_{m2}}$$

- Complex coherence noise model

$$r = \frac{S_1 S_2^*}{\sqrt{|S_1|^2 |S_2|^2}} = \frac{\bar{z}_n n_m N_c e^{j f_x} + (|\mathbf{r}| - N_c \bar{z}_n) e^{j f_x} + (n_{ar} + j n_{ai})}{\sqrt{n_{m1} n_{m2}}}$$

- Multilook estimation

$$\hat{r}_{MLT} = \frac{\bar{z}_n n_m' N_c e^{j f_x} + (|\mathbf{r}| - N_c \bar{z}_n) e^{j f_x} + (n_{ar}' + j n_{ai}')}{\sqrt{n_{m1}' n_{m2}'}}$$

$$E\{n_{ar}'\} = E\{n_{ai}'\} = 0$$

$$E\{n_{m1}'\} = E\{n_{m2}'\} = E\{n_{m2}'\} = 1$$



- Denominator model

$$E\left\{\left\langle |S_1|^2 \right\rangle_{MN} \left\langle |S_2|^2 \right\rangle_{MN} \right\} = \mathbf{y} \left( 1 + \frac{|\mathbf{r}|^2}{MN} \right) \Rightarrow \sqrt{\left\langle |S_1|^2 \right\rangle_{MN} \left\langle |S_2|^2 \right\rangle_{MN}} \approx \mathbf{y} \sqrt{\left( 1 + \frac{1}{MN} \right)}$$

$$\mathbf{r}_{MLT} = \frac{\Delta_{topo} n'_m \exp(j\mathbf{f}_x) + \Delta_{topo} (|\mathbf{r}| - N \bar{c}_n) \exp(j\mathbf{f}_x) + (n'_{ar} + jn'_{ai})}{\sqrt{\left( 1 + \frac{1}{MN} \right)}}$$

- Complex correlation coefficient model

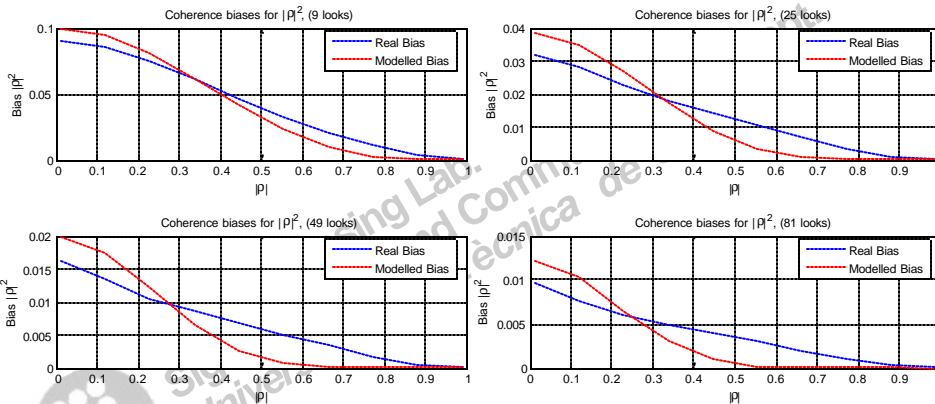
$$\mathbf{r}_{MLT} = |\mathbf{r}| \Delta_{topo} \exp(j\mathbf{f}_x) + \left( 1 + \frac{1}{MN} \right)^{\frac{1}{2}} (n'_{ar} + jn'_{ai})$$

$$E\left\{ |\mathbf{r}_{MLT}|^2 \right\} = |\mathbf{r}|^2 \Delta_{topo}^2 + \left( 1 + \frac{1}{MN} \right)^{-1} \frac{1}{MN} (1 - |\mathbf{r}|^2)^{1.32\sqrt{MN}}$$

$$\Delta_{speckle}^2 = \left( 1 + \frac{1}{MN} \right)^{-1} \frac{1}{MN} (1 - |\mathbf{r}|^2)^{1.32\sqrt{MN}}$$



Simulated data considering no topography



Low coherence bias due to the additive speckle noise component



**Coherence Estimation**      **Non Biased Coherence Estimation**

### Topographic Bias Compensation

Inversion of the underestimation introduced by the topographic component

$$\Delta_{topo} = \left| \frac{1 - \sin\left(\frac{M}{2}w_x\right)}{M \sin\left(\frac{w_x}{2}\right)} \frac{1 - \sin\left(\frac{N}{2}w_y\right)}{N \sin\left(\frac{w_y}{2}\right)} \right|$$

Coherence estimation algorithm

Details

Topography must be estimated from data → **Error source**

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**Coherence Estimation**      **Non Biased Coherence Estimation**

### Filtering via Magnitude Flat Filters

All band-pass filters can not be used as noise is not eliminated, i.e., signal is not correctly estimated

↓

Multiscale filter banks

↓

2D Discrete Wavelet Transform

Coherence estimation algorithm


Details

Topography is **not** estimated from data

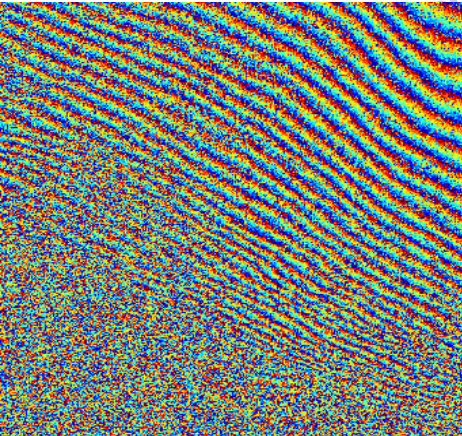
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Coherence Estimation **Non Biased Coherence Estimation**

Mt. Etna (Italy) X-band interferogram acquired by the airborne ESAR system (DE) 

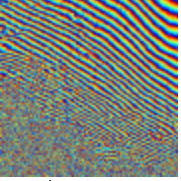
Dimensions: 512x512 pixels

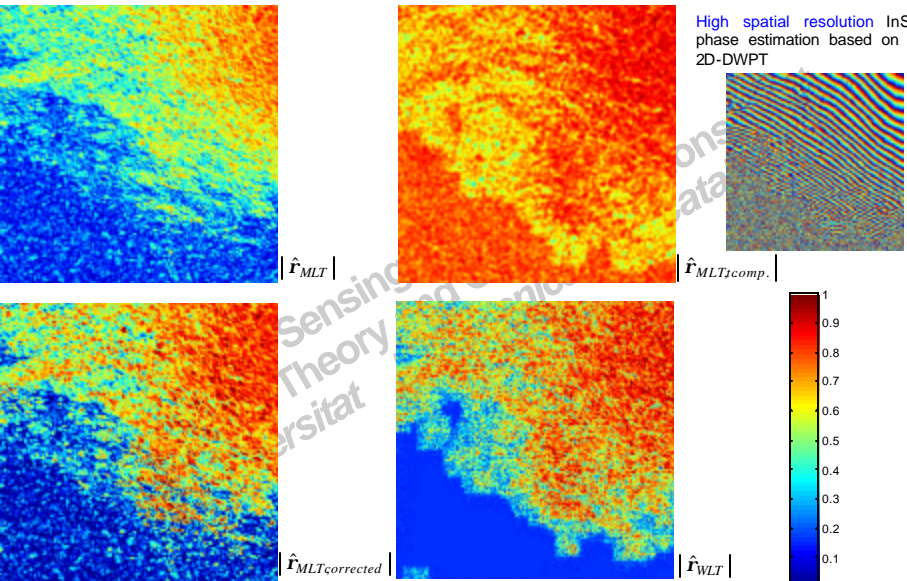


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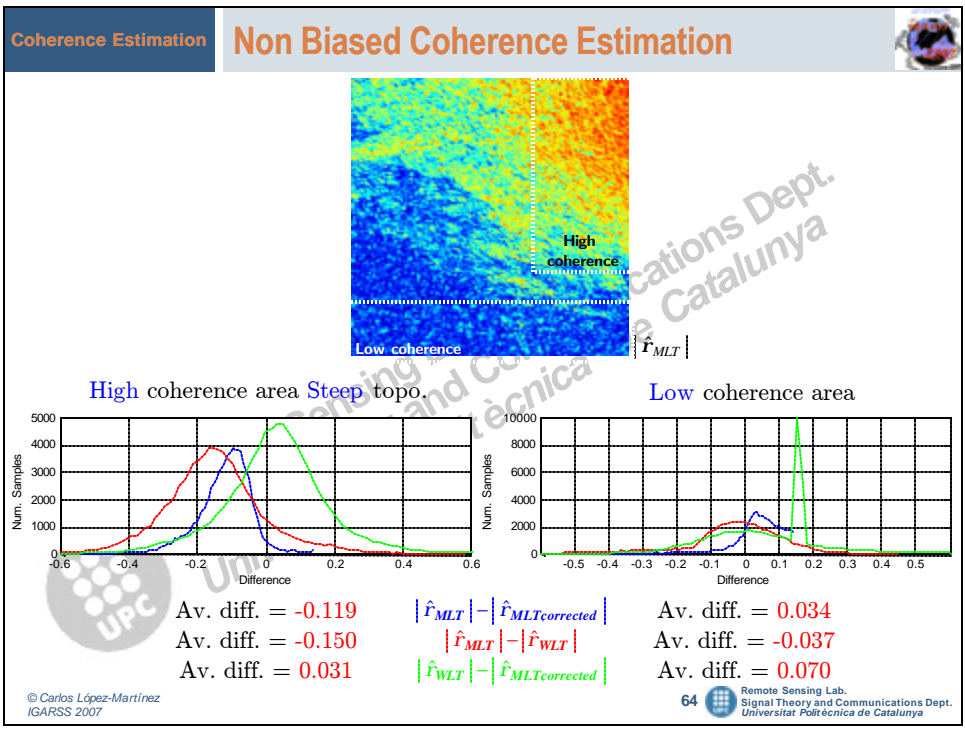
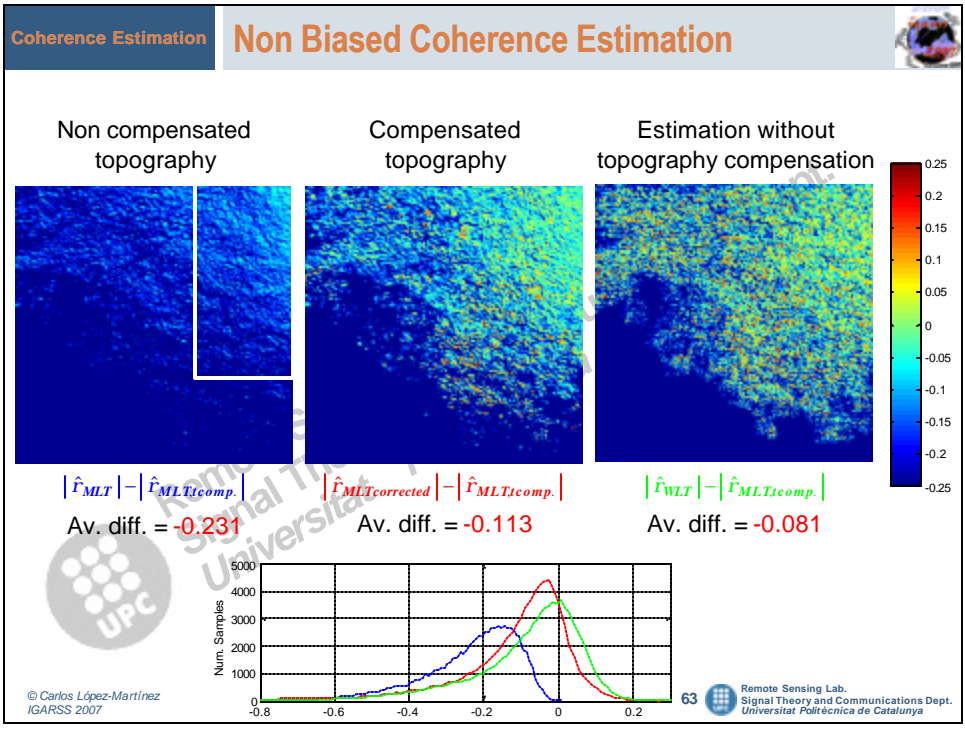
Coherence Estimation **Non Biased Coherence Estimation**

High spatial resolution InSAR phase estimation based on the 2D-DWPT 

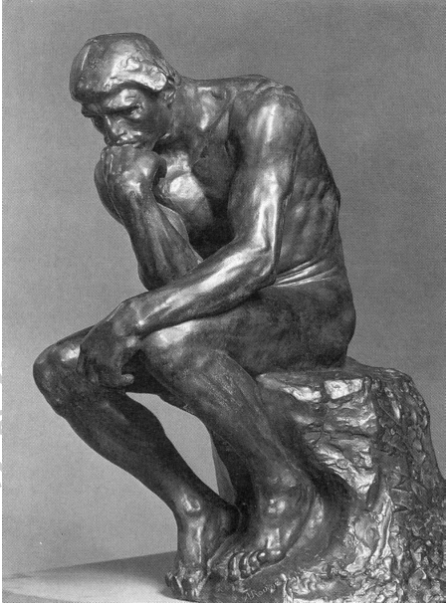


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**Polarimetric Information Estimation**



In SAR polarimetry, incoherent target decomposition theorems, allow the **physical interpretation** of the averaged scattering mechanism in distributed scatterers

- Decomposition theorems represent a way to perform **quantitative remote sensing**

$$E\{\mathbf{k}\mathbf{k}^H\} = \begin{bmatrix} E\{S_{hh}S_{hh}^H\} & E\{\sqrt{2}S_{hh}S_{hv}^H\} & E\{S_{hh}S_{vv}^H\} \\ E\{\sqrt{2}S_{hv}S_{hh}^H\} & E\{2S_{hv}S_{hv}^H\} & E\{\sqrt{2}S_{hv}S_{vv}^H\} \\ E\{S_{vv}S_{hh}^H\} & E\{\sqrt{2}S_{vv}S_{hv}^H\} & E\{S_{vv}S_{vv}^H\} \end{bmatrix} \rightarrow \text{Theoretical average mechanism}$$

$$\langle \mathbf{k}\mathbf{k}^H \rangle = \begin{bmatrix} \langle S_{hh}S_{hh}^H \rangle & \langle \sqrt{2}S_{hh}S_{hv}^H \rangle & \langle S_{hh}S_{vv}^H \rangle \\ \langle \sqrt{2}S_{hv}S_{hh}^H \rangle & \langle 2S_{hv}S_{hv}^H \rangle & \langle \sqrt{2}S_{hv}S_{vv}^H \rangle \\ \langle S_{vv}S_{hh}^H \rangle & \langle \sqrt{2}S_{vv}S_{hv}^H \rangle & \langle S_{vv}S_{vv}^H \rangle \end{bmatrix} \rightarrow \text{Estimated average mechanism}$$

**Depends on the speckle filtering process**



- Monostatic Pauli** scattering vector  $\mathbf{k} = [S_{hh} \quad \sqrt{2}S_{hv} \quad S_{vv}]^T$
- Local** estimate of the coherency matrix  $\mathbf{Z}_n = \frac{1}{n} \sum_{i=1}^n \mathbf{k}_i \cdot \mathbf{k}_i^H = \frac{1}{n} \sum_{i=1}^n \mathbf{Z}_{i,n}$
- Eigenvectors/Eigenvalues analysis of the coherency matrix

$$\mathbf{Z}_n = \mathbf{U}_3 \mathbf{S} \mathbf{U}_3^{-1} = \begin{bmatrix} \mathbf{u}_1 & \mathbf{u}_2 & \mathbf{u}_3 \end{bmatrix} \begin{bmatrix} \mathbf{I}_1 & 0 & 0 \\ 0 & \mathbf{I}_2 & 0 \\ 0 & 0 & \mathbf{I}_3 \end{bmatrix} \begin{bmatrix} \mathbf{u}_1 & \mathbf{u}_2 & \mathbf{u}_3 \end{bmatrix}^H$$

- Eigenvectors are orthonormal
- Eigenvalues are real  $?_1 > ?_2 > ?_3$

$$P_i = \frac{\mathbf{I}_i}{\sum_{k=1}^3 \mathbf{I}_k}$$

Polarimetric Information Estimation **H/A/a Decomposition**

Parametrization of the SU(3) unitary matrix

$$U_3 = \begin{bmatrix} \cos(\mathbf{a}_1) & \cos(\mathbf{a}_2) & \cos(\mathbf{a}_3) \\ \sin(\mathbf{a}_1)\cos(\mathbf{b}_1)e^{id_1} & \sin(\mathbf{a}_2)\cos(\mathbf{b}_2)e^{id_2} & \sin(\mathbf{a}_3)\cos(\mathbf{b}_3)e^{id_3} \\ \sin(\mathbf{a}_1)\sin(\mathbf{b}_1)e^{ig_1} & \sin(\mathbf{a}_2)\sin(\mathbf{b}_2)e^{ig_2} & \sin(\mathbf{a}_3)\sin(\mathbf{b}_3)e^{ig_3} \end{bmatrix}$$

Target 1      Target 2      Target 3

**Decomposition basis**

$I_1$        $I_2$        $I_3$

**Decomposition coefficients**

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Polarimetric Information Estimation **H/A/a Decomposition**

Eigenvalues  $I_1 I_2 I_3$  : Roll Invariant  
 Probabilities  $P_1 P_2 P_3$  : Roll Invariant

ENTROPY      ANISOTROPY

(Degree of Randomness Statistical Disorder)      (Eigenvalues spectrum)

$$H = -\sum_{i=1}^3 P_i \log_3(P_i)$$

$$A = \frac{I_2 - I_3}{I_2 + I_3}$$

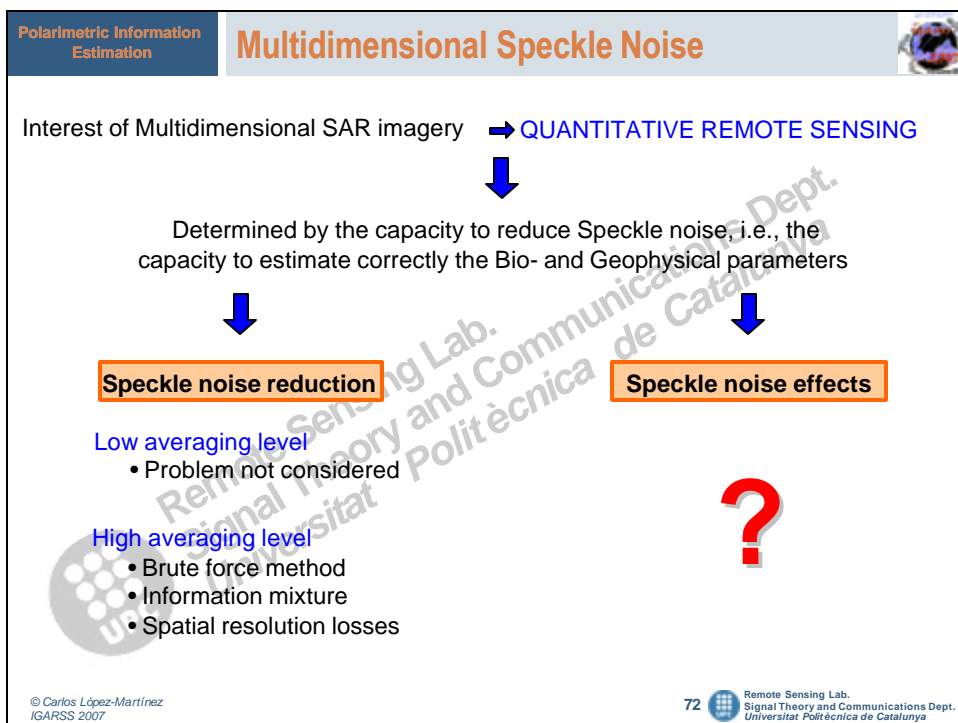
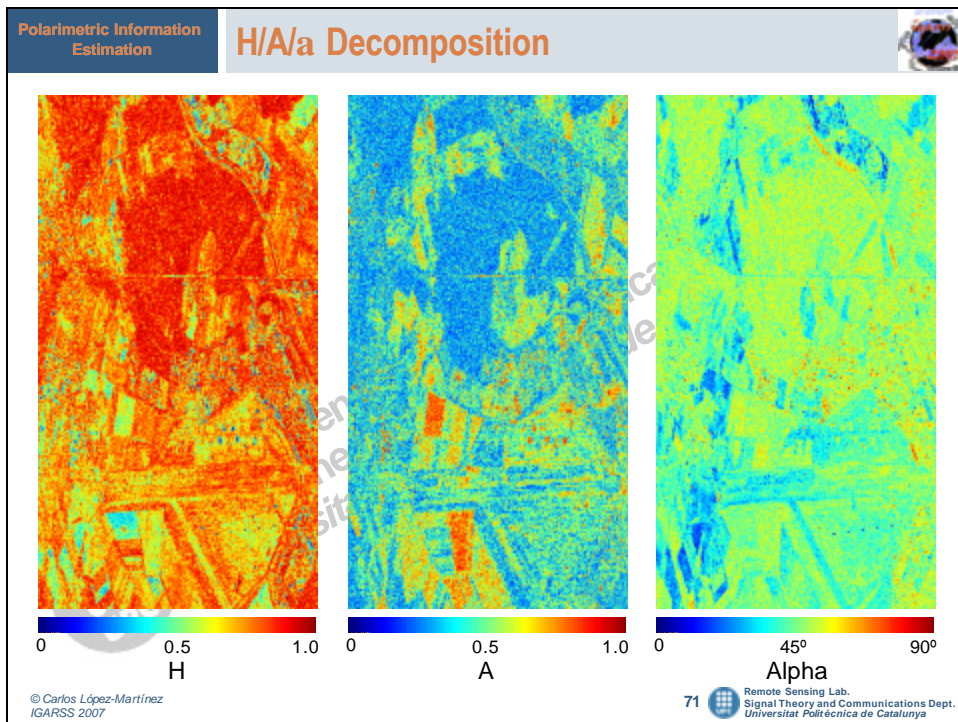
**Pure Target**      **Distributed Target**

$I_1 = SPAN$     $I_2 = 0$     $I_3 = 0$        $I_1 = I_2 = I_3 = SPAN / 3$

$H = 0$        $H = 1$

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Covariance matrix formulism

- Gaussian scattering model for homogeneous areas

$$\mathbf{k} = [S_1, S_2, \dots, S_m]^T$$

$$\mathbf{Z}_n = \frac{1}{n} \sum_{i=1}^n \mathbf{k}_i \mathbf{k}_i^H$$

$$p_{\mathbf{Z}_n}(\mathbf{Z}_n) = \frac{n^m |\mathbf{Z}_n|^{n-m}}{|\mathbf{C}|^n \tilde{\Gamma}_m(n)} \text{etr}(-n\mathbf{C}^{-1}\mathbf{Z}_n)$$

$$S_k = \mathcal{N}_{\mathcal{C}^2}(0, \mathbf{s}^2/2)$$

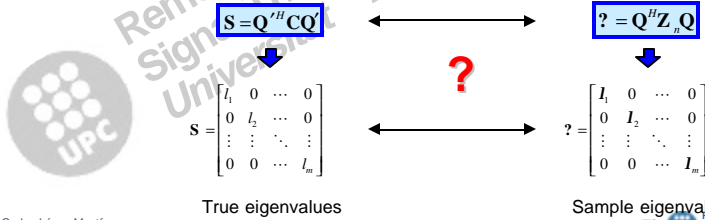
$$\Rightarrow \mathbf{Z}_n \sim \mathcal{W}(n, \mathbf{C})$$

Wishart PDF

Limitations  $\begin{cases} \mathbf{Z}_n, \mathbf{C} & \text{Positive definite} \\ n \geq m \end{cases}$

Two eigenvalue decomposition

- Physical information retrieved via the H/A/a decomposition



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Eigen decomposition transformation

The eigen decomposition can be regarded as a transformation of independent parameters

$$\mathbf{Z}_n = \mathbf{Q} \mathbf{\Lambda} \mathbf{Q}^H$$

↑ Eigenvectors  
↑ Eigenvalues

Jacobian of the transformation found by means of the exterior product of differential forms (skew symmetric product)

$$(d\mathbf{Z}_n) = \prod_{i < j}^m (I_i - I_j)^2 (\mathbf{Q}^H d\mathbf{Q})(d\mathbf{\Lambda}) \quad \infty > I_1 \geq I_2 \geq \dots \geq I_m \geq 0$$

Joint PDF for the eigenvalues/eigenvectors of the matrix  $\mathbf{Z}_n$

$$p_{\mathbf{Q}, \mathbf{\Lambda}}(\mathbf{Q}, \mathbf{\Lambda}) = \frac{n^m \prod_{i=1}^m I_i^{n-m} \prod_{i < j}^m (I_i - I_j)^2}{\tilde{\Gamma}_m(n) \prod_{i=1}^m I_i^n} \text{etr}(-n\mathbf{C}^{-1}\mathbf{Q} \mathbf{\Lambda} \mathbf{Q}^H) (\mathbf{Q}^H d\mathbf{Q})$$

Joint eigenvalues PDF: The dependence on Q must be eliminated

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$$p_r(?) = \frac{p^{m(m-1)} n^{mm} \prod_{i=1}^m I_i^{n-m} \prod_{i<j}^m (I_i - I_j)^2}{\tilde{\Gamma}_m(n) \tilde{\Gamma}_m(m) \prod_{i=1}^m I_i^n} \int_{U(m)} \text{etr}(-nC^{-1}Q?Q^H) (dQ)$$

Joint eigenvalues PDF: Integral expression over U(m)

Group representation theory

Fourier-like analysis of functions in the space U(m) provided by the Group Representation theory

$$p_r(?) = \frac{p^{m(m-1)} n^{mm} \prod_{i=1}^m I_i^{n-m} \prod_{i<j}^m (I_i - I_j)^2}{\tilde{\Gamma}_m(n) \tilde{\Gamma}_m(m) \prod_{i=1}^m I_i^n} {}_0\tilde{F}_0(-nS^{-1}, ?)$$

Complex hypergeometric function of double matrix argument

Joint eigenvalues PDF: Infinite series expression



Soliton theory and τ-functions

τ functions appear as a sort of potential which give rise to the system of N.L.P.D.E. which solution is the soliton.

$$t(n, t, t^*) = \sum_{\kappa, \lambda} K_{\kappa, \lambda} (t) s_{\lambda} (t^*) \Rightarrow t_r(n, t, t^*) = \sum_{\kappa} r_{\kappa}(n) s_{\kappa}(t) s_{\kappa}(t^*) \quad \tau \text{ functions of hypergeometric type}$$

$$t_r(M, X, Y) = {}_p\tilde{F}_q(M + a_1, M + a_2, \dots, M + a_p; M + b_1, M + b_2, \dots, M + b_q; X, Y) \quad \tau \text{ functions of hypergeometric type and matrix argument}$$

Determinant expression for τ functions of hypergeometric type and matrix argument

$$t_r(M, X, Y) = c_m(M) \frac{|t_r(M - m + 1, x_i, y_j)|_{i,j=1}^m}{\Delta(x)\Delta(y)} \quad c_m(M) = \prod_{k=1}^{m-1} (r(M - m + k))^{k-m}, \quad m > 1$$

$$t_r(M - m + 1, x_i, y_j) = 1 + r(M - m + 1)x_i y_j + r(M - m + 1)r(M - m + 2)x_i^2 y_j^2 + \dots$$

Joint sample eigenvalues PDF: Determinant expression

$$p_r(?) = \frac{p^{m(m-1)} n^{\frac{m}{2}(2n-m+1)}}{\tilde{\Gamma}_m(m) \tilde{\Gamma}_m(n)} \prod_{k=1}^{m-1} \left(\frac{1}{k}\right)^{k-m} \frac{\prod_{i=1}^m I_i^{n-m} \prod_{i<j}^m (I_i - I_j)}{\prod_{i=1}^m I_i^m \prod_{i<j}^m (I_j^{-1} - I_i^{-1})} \left| \exp\left(-n \frac{I_j}{I_i}\right) \right|_{i,j=1}^m$$

Sorted sample eigenvalues  $\infty > I_1 \geq I_2 \geq \dots \geq I_m \geq 0$



Joint sample eigenvalues PDF: Simplified expression

$$p_{\lambda}(\lambda) = K(m, n, l_1, \dots, l_m) \prod_{i=1}^m l_i^{n-m} \prod_{i < j} (l_i - l_j) \sum_{\mathbf{p} \in S_m} \text{sgn}(\mathbf{p}) \prod_{i=1}^m \exp\left(-\frac{l_i}{l_{p_i}}\right)$$

$$K(m, n, l_1, \dots, l_m) = \frac{p^{m(m-1)} n^{2n-m+1}}{\Gamma_m(m) \Gamma_m(n)} \frac{\prod_{i=1}^{m-1} l_i^{m-i}}{\prod_{i=1}^m \prod_{j=2}^m (l_i^{-1} - l_j^{-1})}$$

Sorted sample eigenvalues  $\infty > l_1 \geq l_2 \geq \dots \geq l_m \geq 0$

Dependences and analysis of the joint eigenvalues PDF

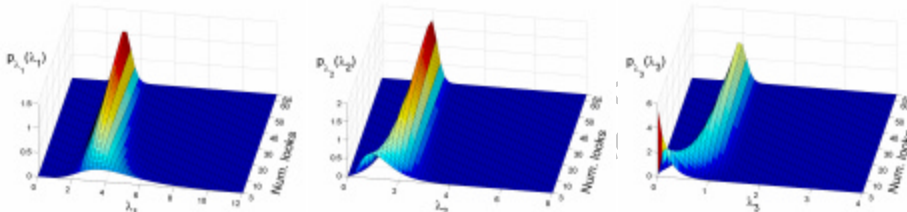
- $n$ : Number of looks. It indicates the effects of the **filtering strength**
- $m$ : Number of channels. Equal to **3** for PolSAR data
- $C, S$ : True information to be retrieved. Important effect over signal **estimation**
- Sample eigenvalues PDF not separable  $\rightarrow$  Sample eigenvalues not independent



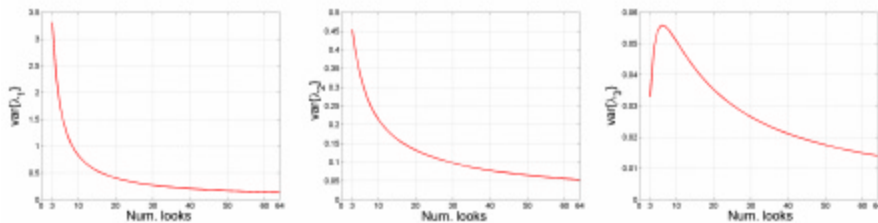
Sample eigenvalues PDFs: Numerical integration

Analytical integration too complex due to the condition  $\infty > l_1 \geq l_2 \geq \dots \geq l_m \geq 0$

Numerical integration (*Gauss quadrature method*) of the case  $\{l_1, l_2, l_3\} = \{3, 2, 1\}$



Sample eigenvalues moments: Numerical integration



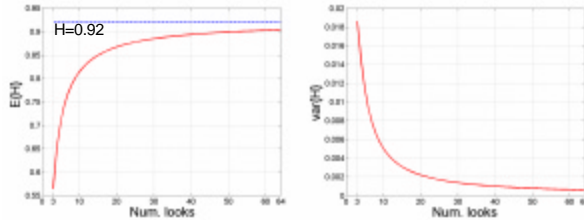
Overestimated

Over/Underestimated

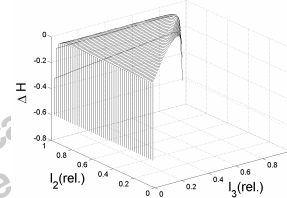
Underestimated



Entropy (H) moments: Numerical integration

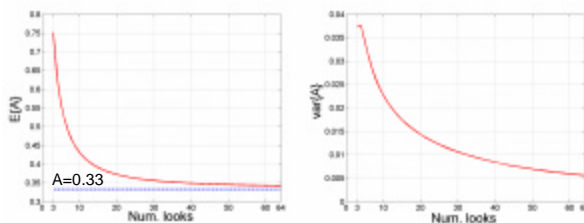


Entropy bias for n=64

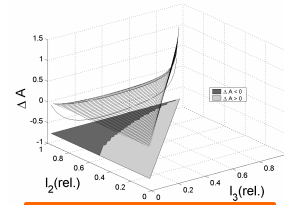


Underestimated

Anisotropy (A) moments: Numerical integration



Anisotropy bias for n=64



Over/Underestimated



Alternative eigenvalues estimation

Classical estimation approach: Maximum Likelihood Approach (MLE)

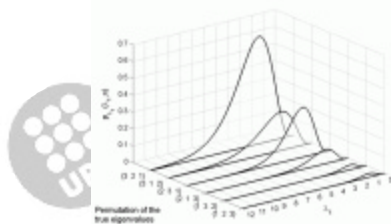
Direct application not possible due to the necessity to maximize a determinant

Asymptotic approach

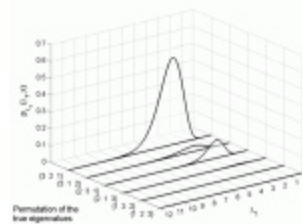
Asymptotic analysis of the sample eigenvalues with respect to the number of looks provided two main results: asymptotic expressions and asymptotic estimation

$$\left| \exp\left(-n \frac{I_i}{I_j}\right) \right|_{i,j=1}^m = \sum_{\mathbf{p} \in S_m} \text{sgn}(\mathbf{p}) \prod_{i=1}^m \exp\left(-n \frac{I_i}{I_{p(i)}}\right) \xrightarrow{n \rightarrow \infty} \prod_{i=1}^m \exp\left(-n \frac{I_i}{I_i}\right)$$

Example for the maximum eigenvalue in three dimensional data (PolSAR)



n=3



n=80



Asymptotic MLE approach

Results in a non-invertible equations system

$$I_i = l_i + \frac{l_i}{n} \sum_{j \neq i}^m \frac{l_j}{l_i - l_j} + O(n^{-1}) \quad i = 1, 2, \dots, m$$

Sample eigenvalues are asymptotic estimators of the true eigenvalues



Speckle noise introduces an asymptotic bias on the sample eigenvalues

Asymptotic quasi MLE (AQ-MLE) approach

Necessity to simplify algebraic expressions in order to find an approximate solution for the equations system



AQ-MLE  $\hat{l}_i = l_i - \frac{l_i}{n} \sum_{j \neq i}^m \frac{l_j}{l_i - l_j} - O(n^{-1}) \quad i = 1, 2, \dots, m$

Drawback: Error in the same order as the eigenvalues correction !!!



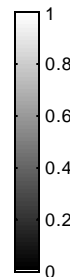
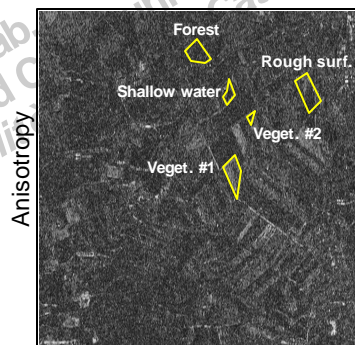
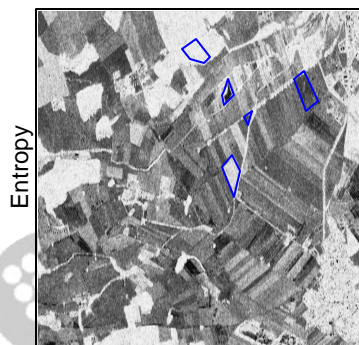
Fully polarimetric L-band dataset acquired with the E-SAR system



Data correspond to the ALLING test-site

Ground truth data available

5 homogeneous areas selected to cover all the Entropy (H) range

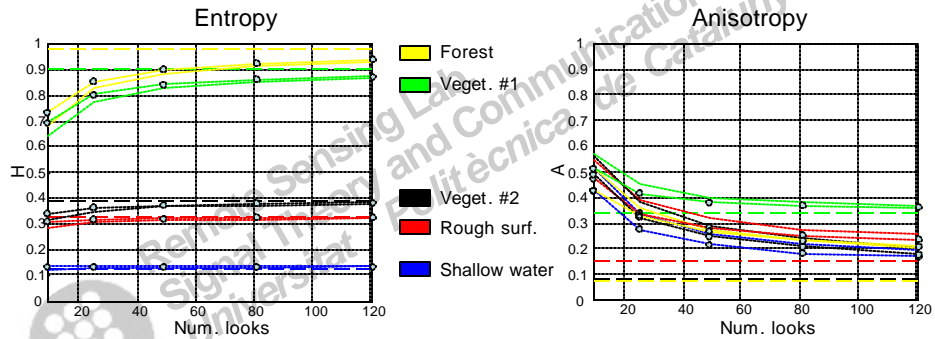




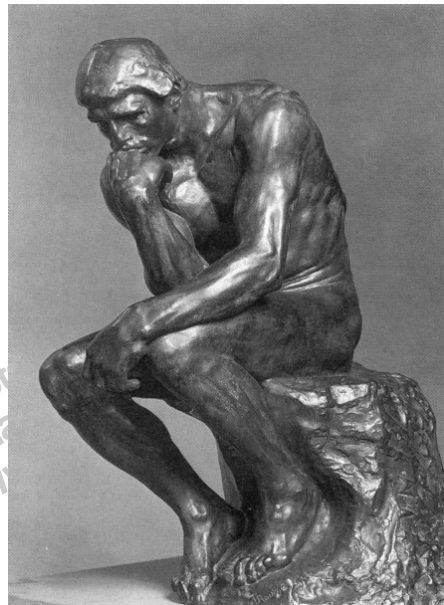
### H/A estimated values

Dependence on the number of looks:  $n \times n$  averaging windows

Dependence on the *true* values of H/A: Average over all the homogeneous area



A minimum number of looks are necessary to retrieve unbiased physical parameters





Multidimensional SAR Data Estimation

Multilook Estimation

Covariance matrix estimation based on a **blind spatial averaging**

- Multilooking
- BoxCar filter

$$\mathbf{Z}_n = \frac{1}{n} \sum_{k=1}^n \mathbf{k}\mathbf{k}^H = \begin{bmatrix} \frac{1}{n} \sum_{k=1}^n S_1(k) S_1^*(k) & \frac{1}{n} \sum_{k=1}^n S_1(k) S_2^*(k) & \cdots & \frac{1}{n} \sum_{k=1}^n S_1(k) S_m^*(k) \\ \frac{1}{n} \sum_{k=1}^n S_2(k) S_1^*(k) & \frac{1}{n} \sum_{k=1}^n S_2(k) S_2^*(k) & \cdots & \frac{1}{n} \sum_{k=1}^n S_2(k) S_m^*(k) \\ \vdots & \vdots & \ddots & \vdots \\ \frac{1}{n} \sum_{k=1}^n S_m(k) S_1^*(k) & \frac{1}{n} \sum_{k=1}^n S_m(k) S_2^*(k) & \cdots & \frac{1}{n} \sum_{k=1}^n S_m(k) S_m^*(k) \end{bmatrix}$$

This filter does not take into account the signal morphology neither speckle noise properties

- Good estimation capabilities = Good speckle noise reduction
- Does not consider neither multiplicative nor additive speckle properties
- Spatial Resolution Loss, blurring edges, erasing thin lines, loss of linear or point features

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Multidimensional SAR Data Estimation **Multilook Estimation**


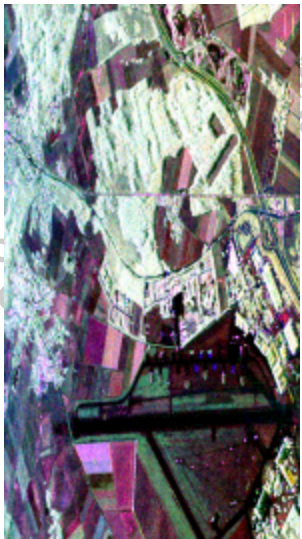
Original RGB 7x7 MLT RGB

$|Shh|$


$|Shv|$

$|Svv|$

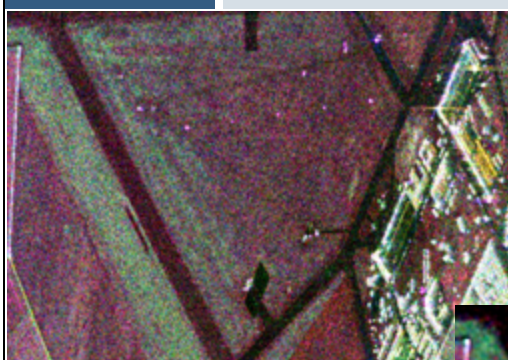



L-band (1.3 GHz) fully PolSAR data  
E-SAR system. Oberpfaffenhofen test area (D)

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Multidimensional SAR Data Estimation **Multilook Estimation**



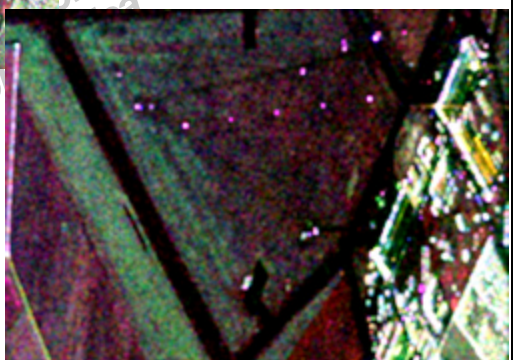
Original RGB



L-band (1.3 GHz) fully PolSAR data  
E-SAR system. Oberpfaffenhofen test area (D)

$|Shh|$   $|Shv|$   $|Svv|$

7x7 MLT RGB



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Considerations about speckle noise reduction



Optical image DLR OP



SAR images reflex the Nature's complexity



SAR image DLR OP

Homogeneous areas

Image details

Heterogeneous areas

Maintain useful information (s)  
RADIOMETRIC RESOLUTION

Maintain spatial details (Shape and value)  
SPATIAL RESOLUTION

Maintain both  
LOCAL ANALYSIS



Local statistics linear filter (Lee filter)

Filter form

$$\hat{I}(x, r) = a E\{I(x, r)\} + b I(x, r)$$

Signal noise model

$$I(x, r) = s(x, r)n(x, r)$$

Minimization criteria (MMSE)

$$\min_{(a,b)} J = E\{|I(x, r) - \hat{I}(x, r)|^2\}$$

MMSE gives

$$a = \frac{1}{E\{n\}} - b$$

$$b = E\{n\} \frac{\text{var}(s)}{\text{var}(I)}$$

$$\hat{I}(x, r) = \frac{E\{I(x, r)\}}{E\{n\}} + b(I(x, r) - E\{I(x, r)\})$$

Statistics need to be derived from noisy data

$$a = \frac{1}{E\{n\}} - b = 1 - b$$

$$b = E\{n\} \frac{\text{var}(s)}{\text{var}(I)} = \frac{\text{var}(I) - E^2\{I\} s_n^2}{\text{var}(I)(1 + s_n^2)}$$

Information estimated from data

$$E\{n\} = 1$$

$$\hat{I}(x, r) = E\{I(x, r)\} + b(I(x, r) - E\{I(x, r)\})$$

Local statistics

$$E^2\{I(x, r)\} \quad \text{var}\{I\}$$

A priori information

$$s_n^2 = \text{var}(n) = \frac{1}{N}$$





$$\hat{I}(x, r) = E\{I(x, r)\} + b(I(x, r) - E\{I(x, r)\})$$

$\text{var}(I) \gg E^2\{I\} \Rightarrow b \rightarrow 1$  Multiplicative noise model can not explain data variability

$\text{var}(I) \approx E^2\{I\} S_n^2 \Rightarrow b \rightarrow 0$  Multiplicative noise model can explain data variability



Original SAR intensity image



Filtered SAR intensity image  
Lee Filter



Filtered SAR intensity image  
Boxcar Filter

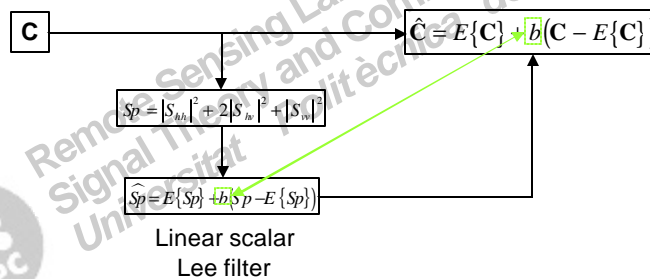


### Polarimetric Lee filter

Nowadays is the most employed polarimetric filtering solution

Extension of the linear scalar Lee filter for SAR images by considering a multiplicative speckle noise model over all the covariance matrix entries

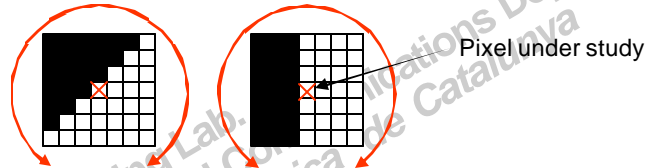
### Working principles





Refined Lee filter

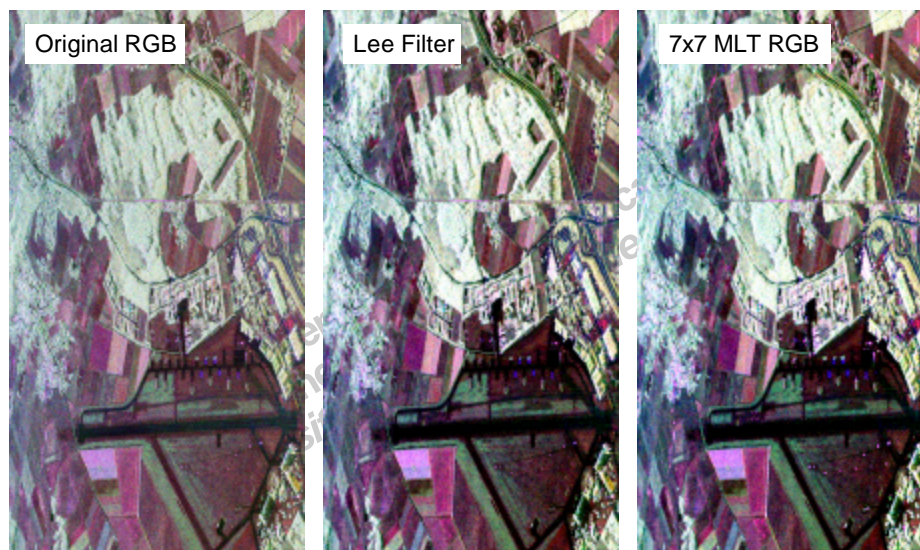
Statistics estimation in windows selected according to the signal morphology in order to retain edges, spatial feature and point targets



The extension of the scalar linear Lee filter presents limitations

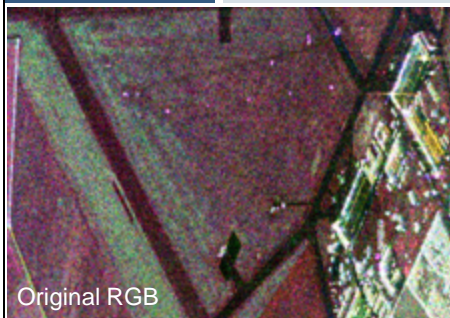
Not based on the multiplicative-additive speckle noise model. This limits the capacity to reduce noise in those images areas characterized by low correlation → The elements of the covariance matrix can be processed differently, but according to the right speckle noise model

The a priori information in the span image  $s_n^2$  is no longer a constant as the noise content in span depends on the data's correlation structure

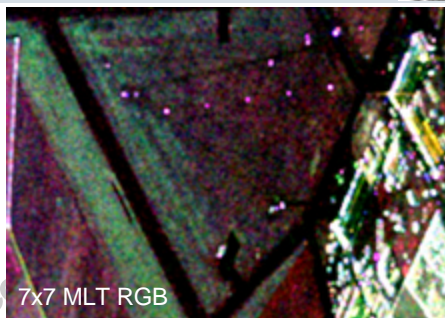


|Shh| |Shv| |Svv|

L-band (1.3 GHz) fully PolSAR data  
E-SAR system. Oberpfaffenhofen test area (D)



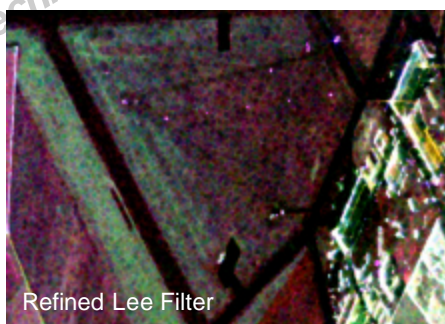
Original RGB



7x7 MLT RGB

$|Shh|$   $|Shv|$   $|Svv|$

L-band (1.3 GHz) fully PolSAR data  
E-SAR system. Oberpfaffenhofen test area (D)



Refined Lee Filter

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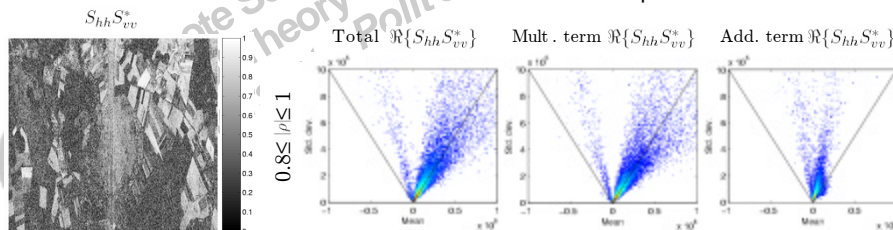
Hermitian product speckle noise model: 
$$S_i S_j^* = \underbrace{y \bar{z}_a n_m N_c e^{j\phi_s}}_{\text{Multiplicativeterm}} + \underbrace{y (|r| - N_c \bar{z}_a) e^{j\phi_s} + y (n_{ar} + j n_{ai})}_{\text{Additiveterm}}$$

C. López-Martínez and X. Fàbregas, "Polarimetric SAR Speckle Noise Model"  
IEEE TGRS, vol. 41, no. 10, pp. 2232 – 2242, Oct. 2003

**Multiplicative speckle noise component:**  $n_m$  → Important for high coherence areas

**Additive speckle noise component:**  $n_{ar} + j n_{ai}$  → Important for low coherence areas

Combination controlled by complex coherence



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Hermitian product speckle noise model:  $\langle S_i S_i^* \rangle_n = \underbrace{y n_m \exp(jf_i)}_{\text{Multiplicative term}} + y (|r| - N_c \bar{z}_n) \exp(jf_i) + y \underbrace{(n_w + j n_a)}_{\text{Additive term}}$

C. López-Martínez and E. Pottier, "Extended multidimensional speckle noise model and its implications on the estimation of physical information," IGARSS 06, Denver (CO) USA, July 2006

### Multiplicative speckle noise component

- Dominant for **high** coherences
- Modulated by phase information

$$E\{n_w\} = N_c \bar{z}_n \quad s_{n_w}^2 = N_c^2 \frac{(1+|r|^2)}{2n}$$

### Additive speckle noise component

- Dominant for **low** coherences
- Not affected by phase information

$$E\{n_w\} = E\{n_a\} = 0 \quad s_{n_w}^2 = s_{n_a}^2 = \frac{1}{2n} (1 - |r|^2)^{1.32} \sigma^2$$

### Effect of the approximations

- Mean value **IS NOT** approximated → No loss of information

$$\lim_{n \rightarrow \infty} \{ y n_m \exp(jf_i) + y (|r| - N_c \bar{z}_n) \exp(jf_i) + y (n_w + j n_a) \} = y |r| \exp(jf_i)$$

- Std. Dev. **ARE** approximated



Define a **multidimensional SAR data filtering strategy** based on the multidimensional speckle noise model

Element to consider: **Covariance matrix**

- ↳ **Diagonal element:** Multiplicative noise source
- ↳ **Non-diagonal element:** Multiplicative and additive noise sources combined according to the complex correlation coefficient





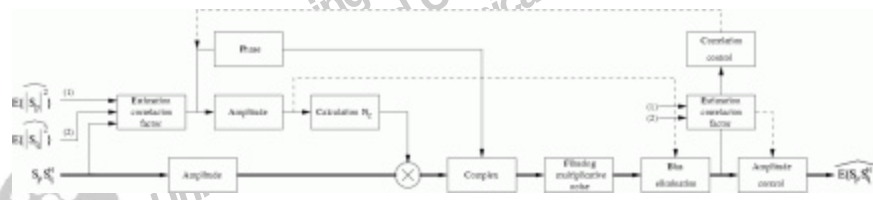
### Diagonal element processing



Any alternative to filter multiplicative noise can be considered  
Non-iterative scheme

### Off-diagonal element processing

The filter uses the Hermitian product speckle model:  $S_p S_p^* = \underbrace{y^* z_c N_a}_{\text{Multiplicative term}} e^{j\phi_c} + \underbrace{y^* (|r| - N_c z_c)}_{\text{Additive term}} e^{j\phi_c} + y^* (n_{ar} + jn_{ia})$



Iterative scheme to take benefit of the improved coherence estimation  
This strategy filters differently the covariance matrix elements



Quantitative evaluation of the filter difficult with experimental SAR data due to speckle



Necessity to consider an evaluation with simulated multidimensional SAR data

The application considered in this paper is: PolSAR data  
Nevertheless results and conclusions may be extended to any multidimensional SAR

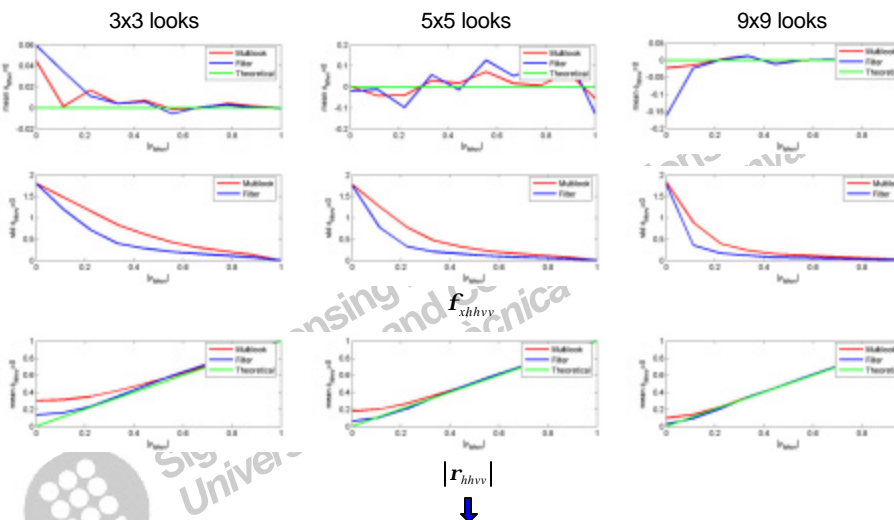
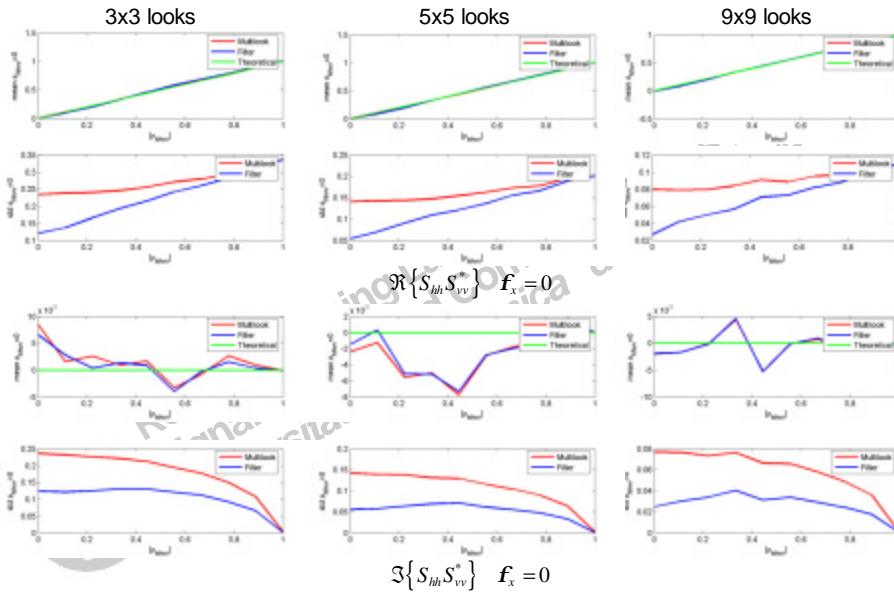
PolSAR data simulated according to the covariance matrix

$$\mathbf{C} = E\{\mathbf{kk}^H\} = \begin{bmatrix} 1 & 0 & |r|e^{j\phi_c} \\ 0 & 0.75 & 0 \\ |r|e^{-j\phi_c} & 0 & 1 \end{bmatrix}$$

Matrix parameterized by the co-polar complex correlation coefficient

Performed tests:

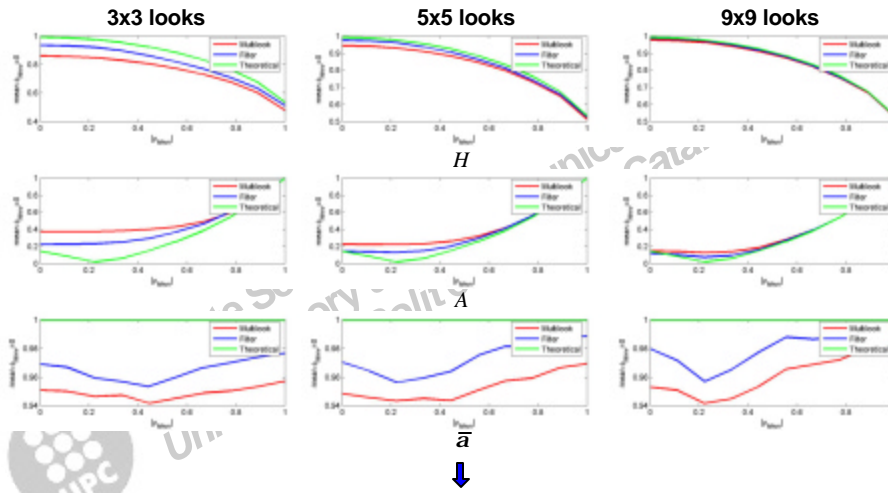
- Covariance matrix elements
- Analysis of: Real and imaginary parts, amplitude, phase, correlation
- Covariance matrix
- Analysis of: Eigendecomposition, polarimetric signatures



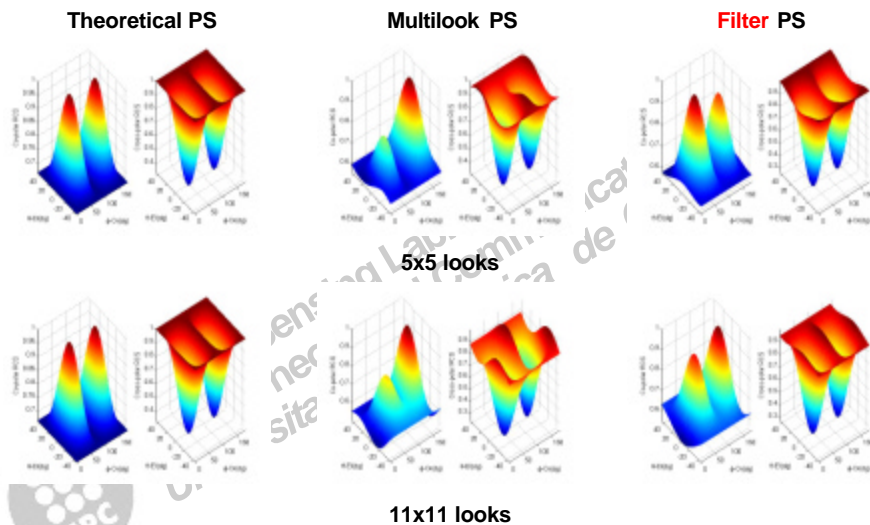
The multidimensional speckle noise model improves the estimation of covariance matrix components, but **what happens with the whole covariance matrix?**



Eigendecomposition applied to the estimated covariance matrices



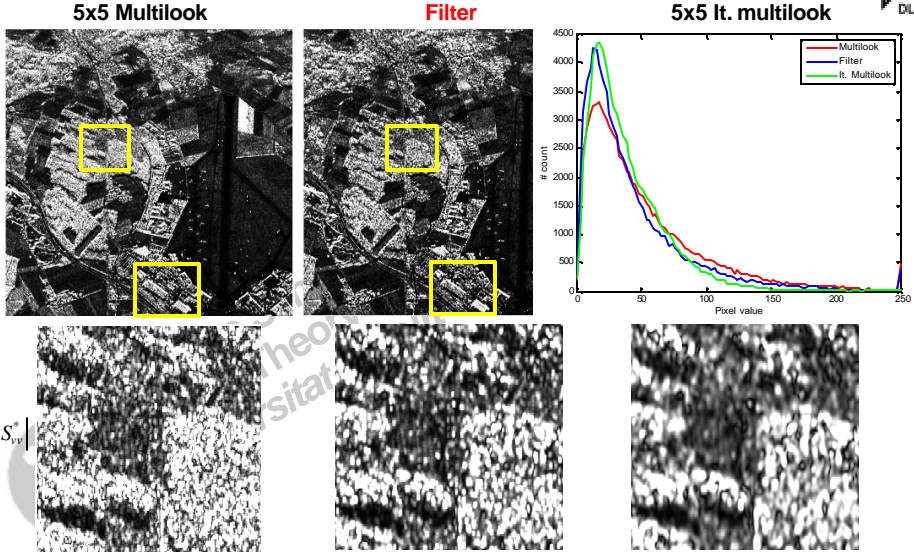
To filter covariance elements differently does not damages information



What happens in this particular case?

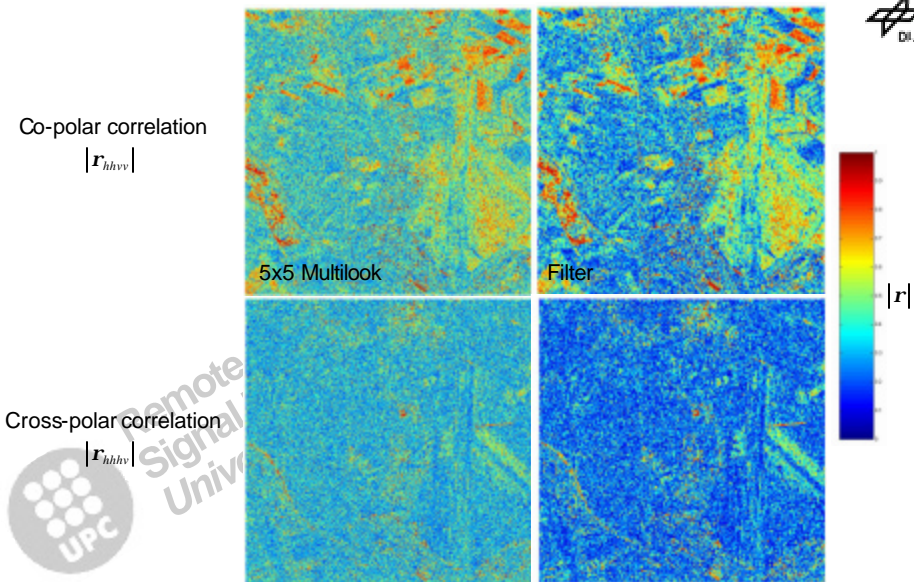


Full-polar ESAR L-Band SAR data in Oberpfaffenhofen (DE)



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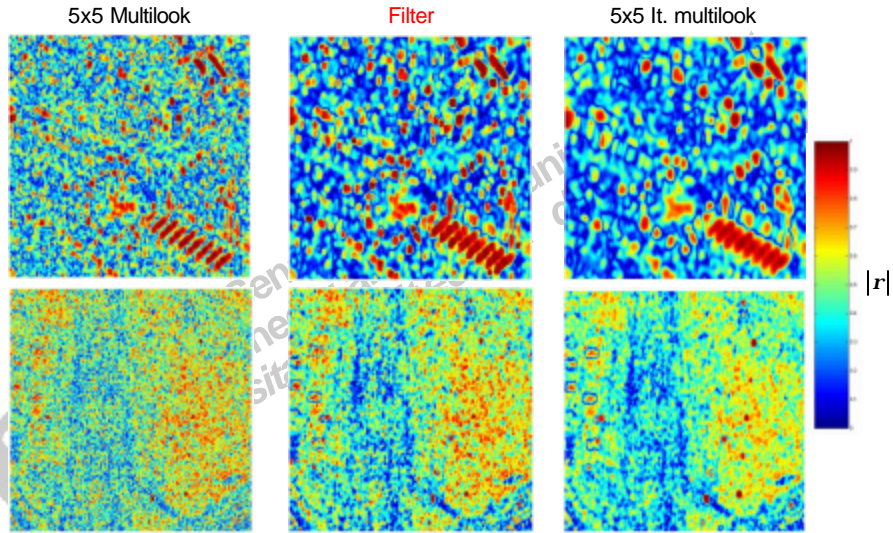
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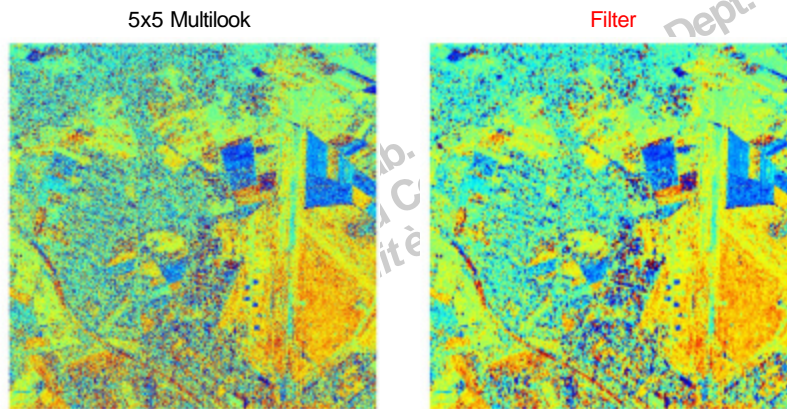


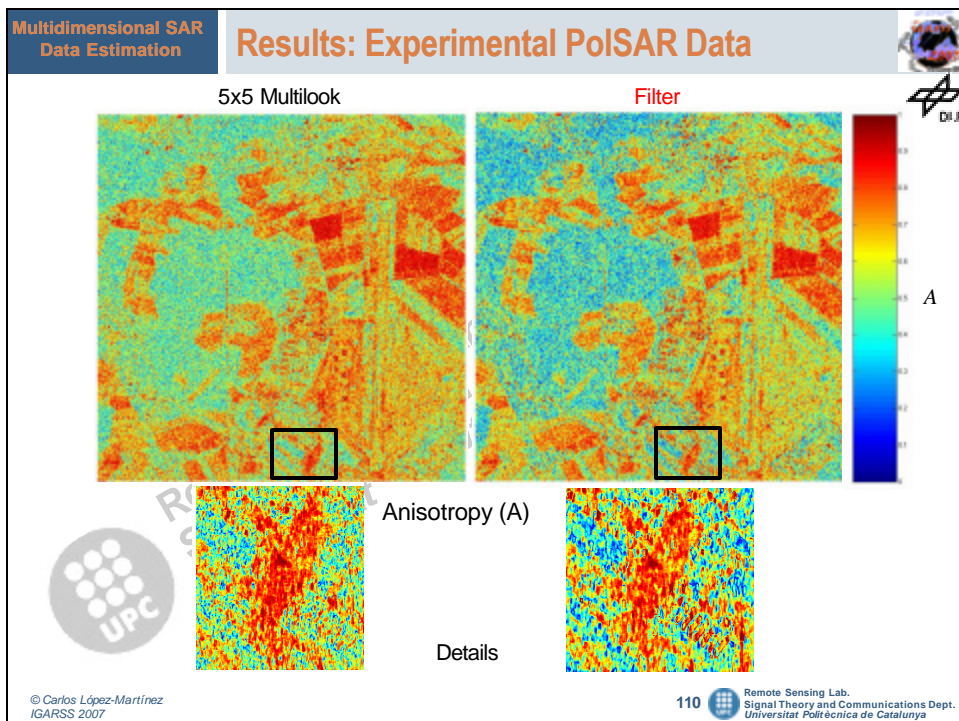
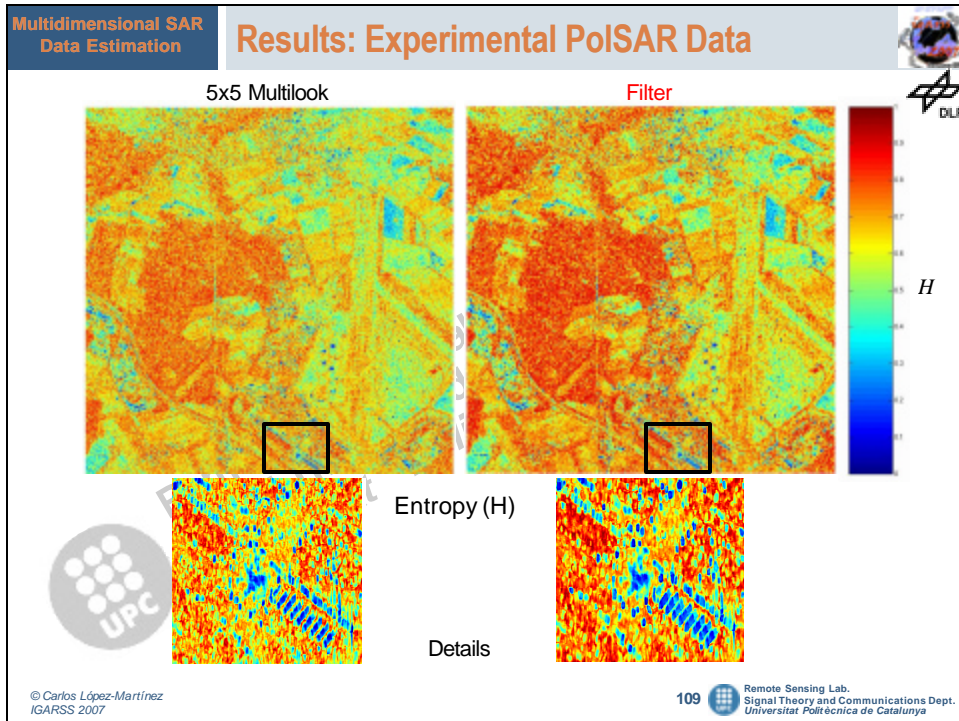
Co-polar correlation  $|r_{hhvv}|$  Details analysis

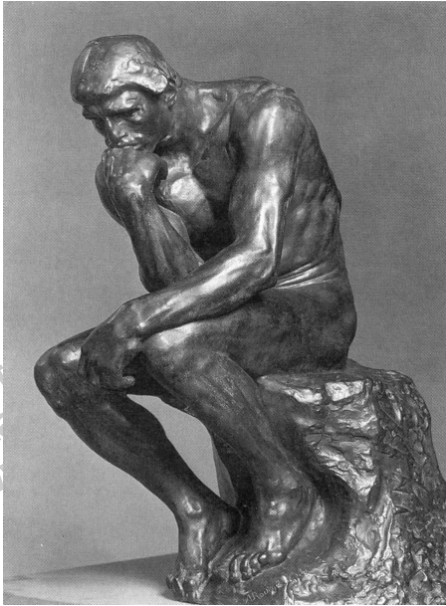


Co-polar correlation phase

$$|r_{hhvv}|$$








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**PollnSAR Data Estimation**

## PolInSAR Data Estimation



Combined use of *Polarimetry* and *Interferometry* to study the scattering centers vertical distribution

$$\mathbf{k}_{p,1} = (1/\sqrt{2}) [S_{HH+VV,1}, S_{HH+VV,1}, 2S_{HV,1}]^T$$

$$\mathbf{k}_{p,2} = (1/\sqrt{2}) [S_{HH+VV,2}, S_{HH+VV,2}, 2S_{HV,2}]^T$$

$$\Rightarrow \mathbf{k}_6 = \begin{bmatrix} \mathbf{k}_{p,1} \\ \mathbf{k}_{p,2} \end{bmatrix} \Rightarrow \mathbf{T}_6 = \frac{1}{n} \sum_{i=1}^n \mathbf{k}_6 \mathbf{k}_6^H = \begin{bmatrix} \mathbf{T}_{11} & \mathbf{T}_{12} \\ \mathbf{T}_{12}^H & \mathbf{T}_{22} \end{bmatrix}$$

Estimation process

The capability to explore the *polarizations space* allows to consider the idea to *optimize* interferometric coherences

$$r(\mathbf{w}_1, \mathbf{w}_2) = \frac{\mathbf{w}_1^H \mathbf{T}_{12} \mathbf{w}_2}{\sqrt{\mathbf{w}_1^H \mathbf{T}_{11} \mathbf{w}_1 \mathbf{w}_2^H \mathbf{T}_{22} \mathbf{w}_2}}$$

Optimization process

$$L = \mathbf{w}_1^H \mathbf{T}_{12} \mathbf{w}_2 + L_1(\mathbf{w}_1^H \mathbf{T}_{11} \mathbf{w}_1) + L_2(\mathbf{w}_2^H \mathbf{T}_{22} \mathbf{w}_2)$$

$$\mathbf{T}_{22}^{-1} \mathbf{T}_{12}^H \mathbf{T}_{11}^{-1} \mathbf{T}_{12} \mathbf{w}_2 = \mathbf{u} \mathbf{w}_2$$

$$\mathbf{T}_{11}^{-1} \mathbf{T}_{12} \mathbf{T}_{22}^{-1} \mathbf{T}_{12}^H \mathbf{w}_1 = \mathbf{u} \mathbf{w}_1$$

$$\mathbf{u} = \hat{L}_2^*$$

Optimum coherences  $|r|_{opt} = \sqrt{\mathbf{u}}$

Optimum eigenvectors  $\mathbf{w}_{1,opt} \quad \mathbf{w}_{2,opt}$

## PolInSAR Data Estimation

## Speckle Noise Effects



How does *speckle* affect *optimum* coherences and *optimum* eigenvectors?

R. T. Fomena and S. R. Cloud, "On the role of coherence optimization in polarimetric SAR interferometry," CEOS SAR workshop, Adelaide, Australia, Sept. 2005.

Optimum parameters are affected by the processes

Estimation process

$$\mathbf{Z}_n = \mathbf{C} + \Delta \mathbf{Z} = \mathbf{C} + \mathbf{N}_M + \mathbf{N}_A$$

Optimization process

$$\hat{I}_i = I_i - \frac{1}{n} \sum_{j \neq i} \frac{I_j}{I_i - I_j} - O(n^{-1}) \quad i = 1, 2, \dots, m$$

$$\mathbf{T}_{22}^{-1} \mathbf{T}_{12}^H \mathbf{T}_{11}^{-1} \mathbf{T}_{12} \mathbf{w}_2 = \mathbf{u} \mathbf{w}_2$$

$$\mathbf{T}_{11}^{-1} \mathbf{T}_{12} \mathbf{T}_{22}^{-1} \mathbf{T}_{12}^H \mathbf{w}_1 = \mathbf{u} \mathbf{w}_1$$

Degrees of freedom/dependence

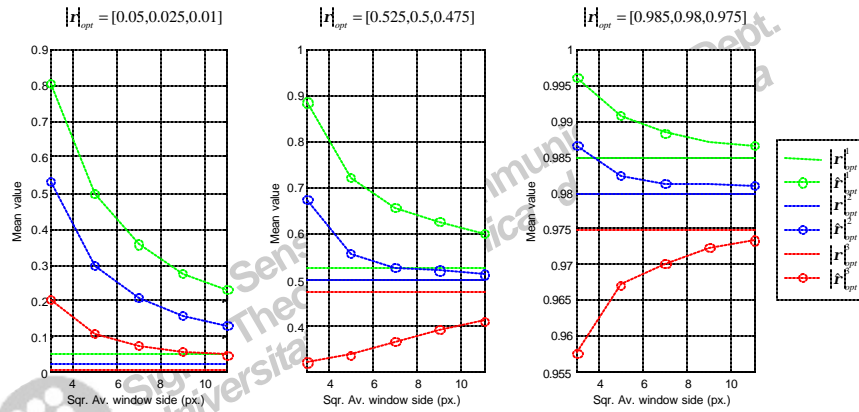
$$\begin{cases} \mathbf{T}_{11} \quad \mathbf{T}_{22} & \text{PolSAR information} \\ \mathbf{T}_{12} & \text{PolInSAR information} \end{cases}$$



Analysis and study based on simulated data  
Under the *Gaussian* hypothesis

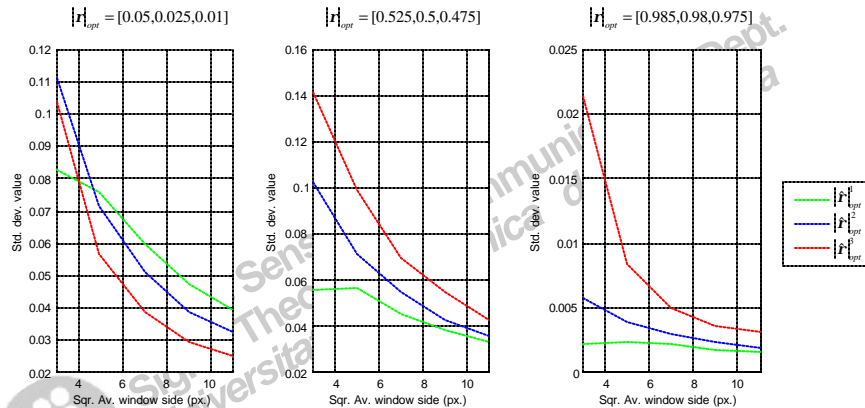


## Optimum coherence *mean value* vs. optimum coherence *exact value*



Estimated optimum coherences

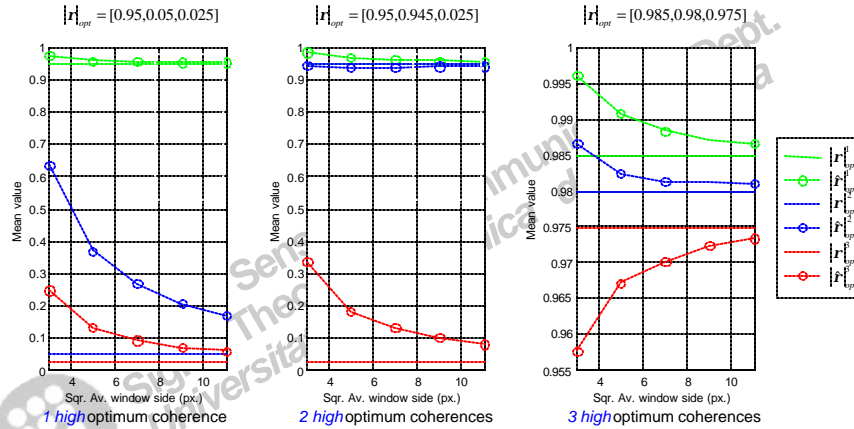
- Asymptotically non-biased
- Over- or underestimation
- Depend on the corresponding exact values, but also on the other optimum coherences



- Std. Dev. decreases with the number of averaged samples
- Not clear behaviour of the Std. Dev. Value
  - Higher values for medium optimum coherences
  - It appears that Std. Dev. is inversely proportional to the optimum coherence value



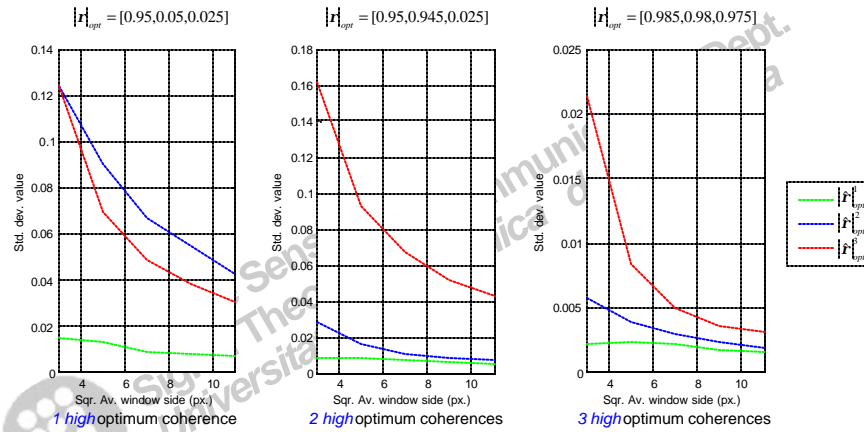
Optimum coherence **mean value** vs. number of optimum coherences presenting high values



- High optimum coherences are robust
  - Different behaviour respect to the sample eigenvalues in PoliSAR due to an *amplitude limitation*
- Over- or underestimation depending of the optimum coherences spectra

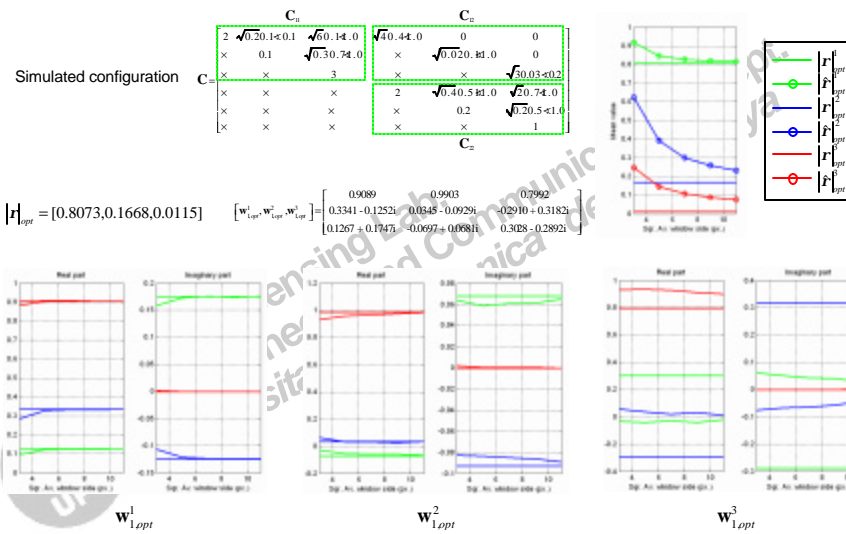


Optimum coherence **Std. Dev.** vs. number of optimum coherences presenting high values

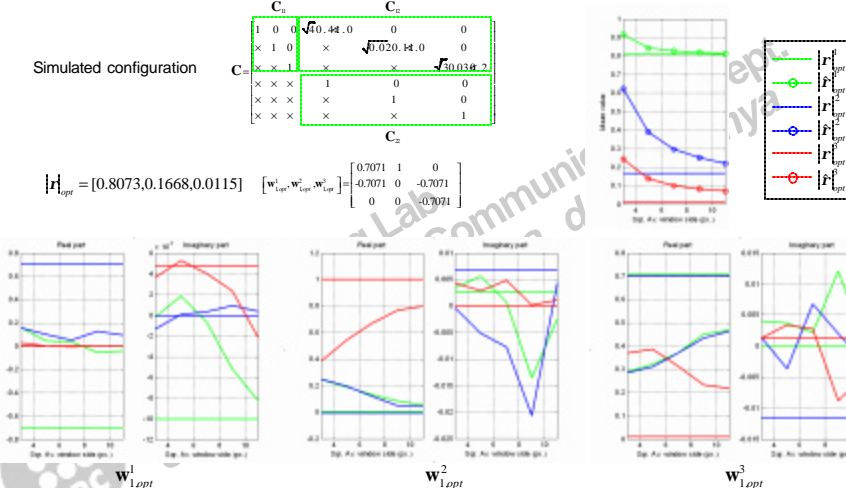




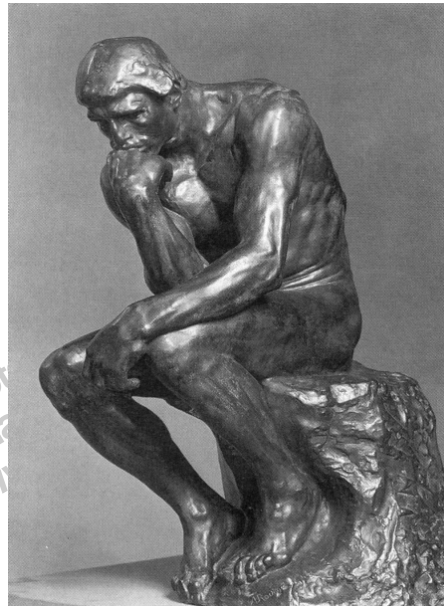
## Optimum eigenvectors vs. PolSAR datasets structure



## Optimum eigenvectors vs. PolSAR datasets structure



- Optimum eigenvectors affected by the internal structure of the PolSAR datasets
  - Possible influence of the speckle additive noise component (important for low coherences)



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